INDEPENDENT TECHNICAL REPORT, EUREKA RARE EARTH PROJECT, NAMIBIA

Prepared For

Battery Road Capital Corp.

Effective Date:	**2 August 2021**
Signature Date:	**10 September 2021**

Qualified Persons:

Martin Pittuck	**CEng, FGS, MIMMM**
Keith Webb	**MAIG**

Report Prepared by

srk consulting

SRK Consulting (UK) Limited
UK30999

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Date:		September 2021
Project Number:		UK30999
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Contributing Author	Keith Webb MAIG	*signed*
Peer Reviewer	Mike Armitage PhD, C.Eng, C.Geol	*signed*

CERTIFICATE OF QUALIFIED PERSON

I, Martin Frank Pittuck, MSc., C.Eng, MIMMM do hereby certify that:

1. I am a Corporate Consultant of SRK Consulting (UK) Limited, 5th Floor, Churchill House, 17 Churchill Way, Cardiff, CF10 2HH, Wales, UK
2. The Technical Report to which this certificate applies is titled “Independent Technical Report, Eureka Rare Earth Project, Namibia” With an effective date of 02 August 2021 prepared for Battery Road Capital Corp..
3. I am a graduate with a Master of Science in Mineral Resources gained from Cardiff College, University of Wales in 1996 and I have practised my profession continuously since that time. Since graduating I have worked as a consultant at SRK on a wide range of mineral projects, including many gold deposits. I have undertaken many geological investigations, resource estimations, mine evaluation technical studies and due diligence reports. I am a Professional Member of the Institution of Materials Mining and Metallurgy (Membership Number 49186), a Fellow of the Geological Society of London and I am a Chartered Engineer;
4. I have read the definition of “Qualified Person” set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfil the requirements to be a “Qualified Person” for the purposes of NI 43-101.
5. I have not visited the Eureka Project.
6. I am responsible for all sections of this Technical Report except for sections 2, 4, 5 and 7.
7. I am independent of Battery Road Capital Corp. and the Eureka property as described in Section 1.5 of NI 43-101.
8. I have had no prior involvement with the properties that are the subject of this Technical Report.
9. I have read NI 43-101 and the parts of the Technical Report that I am responsible for have been prepared in compliance with NI 43-101.
10. As of the effective date of the Technical Report, to the best of my knowledge, information and belief, the parts of the Technical Report that I am responsible for contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated this 10th day of September 2021.

Signed

Martin Pittuck (CEng, FGS, MIMMM)
Corporate Consultant (Mining Geology)
SRK Consulting (UK) Limited

CERTIFICATE OF QUALIFIED PERSON

I, Keith Webb, MAIG, do hereby certify that:

1. I am an independent consulting/contract geologist 148 Eros Road, Eros Park, Windhoek, Namibia, 10009.
2. The Technical Report to which this certificate applies is titled "Independent Technical Report, Eureka Rare Earth Project, Namibia" With an effective date of 02 August 2021 prepared for Battery Road Capital Corp.
3. I hold a BSc Honours in Applied Geology from the University of Strathclyde, Scotland, 1985. I have been involved in mining and exploration geology for the past 35 years and have extensive experience within West, East and Southern Africa, as well as Turkey, covering a range of commodities including Gold, Copper, Nickel, Lead/Zinc, Uranium, and Diamonds. I am a member of the Australian Institute of Geoscientists (Member ID 3688) and currently sit on the committee for the Geological Society of Namibia.
4. I have read the definition of "Qualified Person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfil the requirements to be a "Qualified Person" for the purposes of NI 43-101.
5. I visited the Eureka Project on 23rd June 2020 and 26th July 2021.
6. I am responsible for sections 2, 4, 5 and 7 of this Technical Report.
7. I am independent of Battery Road Capital Corp. and the Eureka property as described in Section 1.5 of NI 43-101.
8. I have had no prior involvement with the properties that are the subject of this Technical Report.
9. I have read NI 43-101 and the parts of the Technical Report I am responsible for, and the parts of the Technical Report that I am responsible for have been prepared in compliance with NI 43-101.
10. As of the effective date of the Technical Report, to the best of my knowledge, information and belief, the parts of the Technical Report that I am responsible for contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated this 10th day of September 2021.

Signed

Keith Webb (MAIG)

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INDEPENDENT TECHNICAL REPORT, EUREKA RARE EARTH PROJECT, NAMIBIA

1 SUMMARY

1.1 Overview

SRK Consulting (UK) Ltd. (“SRK”) has been asked by Battery Road Capital Corp. (“Battery Road”, the “Company” or the “Client”) to review the Eureka Rare Earth Element (“REE”) Project in Namibia (“Eureka” or the “Project”) owned 100% by E-Tech Kalapuse Mining (Pty) Limited (“E-Tech Namibia”). This resulting Independent Technical Report (“ITR”) has been prepared in accordance with National Instrument 43-101 (“NI 43-101”).

The ITR will be used in support of a reverse take-over (“RTO”) of E-Tech Namibia by Battery Road which is currently listed on the TSX Venture Exchange (TSXV:BTRY.P). The Transaction also contemplates a concurrent private placement) by Battery Road to further support on-going exploration activities by E-Tech Namibia of $5,000,000 on market terms.

This ITR describes the work undertaken to produce a maiden Mineral Resource estimate for the Project which was originally prepared by SRK on behalf of E-Tech Metals Ltd and the metallurgical testwork results obtained to date as well as describing the project geology, location and ownership. The ITR also describes the merits of the project, the challenges remaining to be faced and the Company’s proposed development programme.

1.2 Location

The project area is semi-arid desert in the Karibib District of the Erongo Region, Namibia as shown in Figure 1-1. The Trans-Kalahari highway passes within 2 km of the project site providing direct access to the capital Windhoek as well as port facilities at Walvis Bay. The Project is 250 km by road from the capital Windhoek, a journey of approximately 2.5 hours.

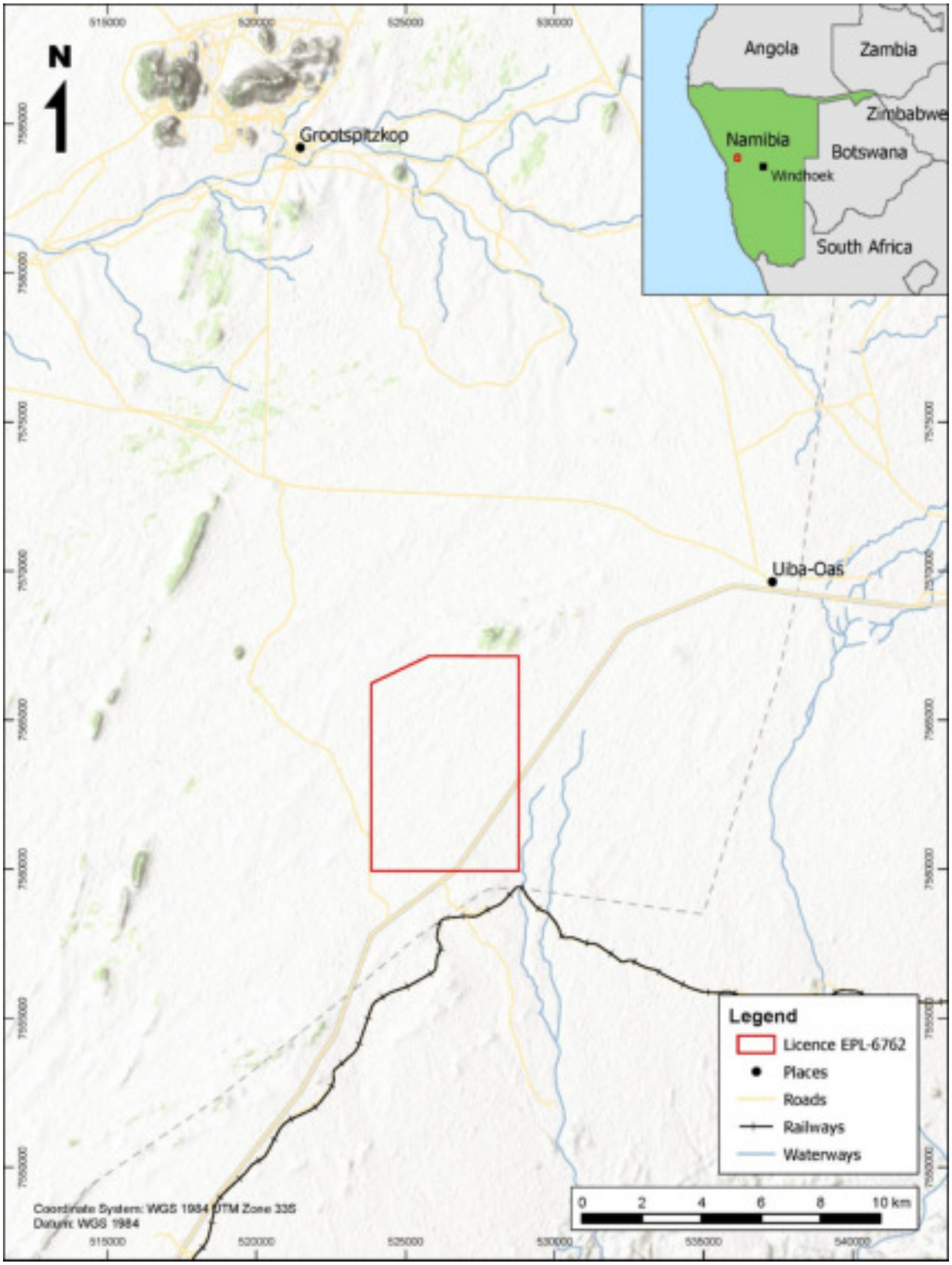

Figure 1-1: Project Location

1.3 Licence Description, Ownership and Terms

The Eureka deposit lies within Exclusive Prospecting Licence ("EPL") number EPL 6762; which covers Eureka Farm 99 and Sukses Farm 90 and encompasses a roughly rectangular area totalling 3,474 ha.

The previous licence holder, KALAPUSE GENERAL DEALERS cc ("KGD") agreed to excise the Eureka licence area from its EPL 5469 licence area with the consent of Namibia's Ministry of Mines & Energy in a letter received on 15 June 2017.

EPL 6762 was then awarded to E-Tech Namibia on 12th February 2018 for an initial 3 year duration; and for the exploration of base and rare metals, industrial minerals, nuclear fuel minerals and precious metals until 12th February 2021. The licence was renewed on 20th July, 2021 until 19th July, 2023, and will be renewable from 19th July 2023 for another two year period. Additional licence renewals, beyond seven years, are possible with approval from the Minister of Mines and Energy.

At the time KGD ceded rights to E-Tech Namibia, a non-refundable consideration of GBP 7,500 (VAT excluded) was paid by E-Tech Namibia to KGD. and one half of the second non-refundable consideration of GBP 7,500 was paid in November 2020 with the remaining half scheduled to be paid on completion of the RTO transaction.

Upon the successful conclusion of a prefeasibility study ("PFS") and progression towards definitive feasibility studies and mine development, E-Tech Namibia is required to pay a further non-refundable consideration of GBP 50,000 (VAT excluded) to KGD. This has not yet been paid.

In addition, E-Tech Namibia pays under contract Early Prospecting Stage farmer compensation of NAD 2,500 per month.

1.4 Geology and Mineralisation

The Project is located within the Southern Central Zone of the Neoproterozoic Damara Belt. The intrusive that hosts the mineralisation at Eureka was emplaced at a similar time to the regional granites, it is the only currently known alkaline intrusion related to the Damara Orogeny.

At least 14 REE-bearing dolomite carbonatite dykes have been identified at Eureka, these are found in four Zones within several hundred metres of each other. The dykes intrude quartzo-feldspathic and calc-silicate rocks of the Etusis and Khan formations respectively. These dykes are generally greater than 0.5 m thick and are principally composed of coarse dolomite with a variable abundance of coarse monazite (the host of the REEs), magnetite, graphite, calcite, hematite and minor quartz. Locally, the dykes are surrounded by a thin selvage of skarn-like rock comprising diopside, actinolite, monazite, and graphite.

1.5 Work Completed by E-Tech

1.5.1 Exploration

During Q4 2016 a ground magnetic and radiometric survey was completed which, combined with known carbonatite outcrops, generated a number of drill targets. In March 2017 E-Tech Namibia completed 19 reverse circulation ("RC") drillholes for a total of 610 m in Zones 1, 2 and 3. Following this, a gravity orientation study was completed in Q3 2017 which added further exploration targets.

During Q2 2019, 1.2 km of trenching was completed on Zones 1, 2 and 3 and reconnaissance mapping found new mineralised float samples south of Zone 3 and in Zone 4.

At this time an aerial topographic imagery survey was also carried out, covering an area of approximately 1.5 x 1.0 km, centred on the known mineralisation in Zones 1, 2, 3 and 4.

1.5.2 Drilling

Initially, 19 RC drillholes for 613m were completed mostly on Zone 1 and 2 with a few in Zone 3; these have been sampled and assayed and have been used in the Mineral Resource estimate given in this Technical Report.

In late 2020 and the first half of 2021, another 23 RC drillholes were completed for 3,305m; these provide some infill holes in Zone 1 and significantly improved drilling coverage in Zone 3.

In June 2021 a 5-hole diamond drilling programme was completed, these provide deep intersections in Zone 1 and 2.

None of the 2020-2021 drilling has been assayed at this stage.

1.5.3 Metallurgy and Processing

During Q4 2016, E-Tech Namibia collected a 300 kg bulk sample of fresh carbonatite from Zone 1 for metallurgical testing. A representative 100 kg crushed split of this sample was submitted to SGS Mineral Services in the UK. Monazite liberation and gravity separation was studied over a range of size fractions. A first-pass recovery of 65% to gravity concentrate was achieved and subsequent magnetic separation of the dry gravity concentrate improved its grade from 47% to 59% total rare earth oxide ("TREO") without loss of monazite.

The original concentrates produced by SGS were analysed at Wheal Jane Laboratories using an ICP-OES method which does not assay Th and U accurately. Therefore, a number of samples of the gravity and magnetic separation concentrates were submitted to Actlabs (Canada) for umpire analysis using ICP-MS which provided comparable REE grades and significantly lower values for Th and U resulting in values in the expected range based on previous Laser Ablation Induced Coupled Plasma Mass Spectrometry ("LA-ICPMS") work.

During Q4 2019 E-Tech Namibia collected a 1 t bulk sample of fresh carbonatite from a test pit for further metallurgical testing by Bond Equipment of Klerksdorp, South Africa. The aim of this testwork was to further develop and optimise the processing flowsheet design for a potential gravity plant at Eureka.

1.5.4 Density

Density measurements have been collected for 21 grab samples of fresh mineralised carbonatite and waste rock.

1.5.5 Geological Modelling

E-Tech Namibia engaged the services of Impala Geomodelling LTD ("Impala") to create a geological model based on surface mapping, lithological logging and assay data. Fourteen carbonatite dykes were modelled with a combined strike length of over 1,200 m. The dykes dip steeply, trend E-W to NW-SE and have been drill tested to a depth of up to 60 m below surface where they remain open along strike and at depth. The dykes are between 0.5 m and 5 m thick (averaging approximately 2 m thick), have sharp lithological contacts with the host rock which act as a natural cut-off grade of around 1% TREO and suggest that potentially economic mineralisation is contained entirely within the dykes, not in a metasomatic alteration halo around the dykes.

Weathering surfaces have not been produced as the base of weathering is shallow and not considered to be material to the Mineral Resource estimate.

1.5.6 Mineral Resource Estimation

Baker Geological Services Ltd (“BGS”) prepared a 3D block model for the Project and undertook statistical and geostatistical studies to determine appropriate interpolation parameters.

Grades of TREO%, and where possible, Th, U, La, Ce, Pr, Nd, Sm, Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb, Lu, Sc and Y were then interpolated into the empty block model using Ordinary Kriging (“OK”) with the following post estimation processes being completed:

- Slope of Regression calculation to enable an assessment of the quality of the estimate;
- Conversion of all REE to oxides;
- Calculation of the combined LREOs; and
- Calculation of the combined HREOs.

The resulting block model grades were validated through visual and statistical methods with the input data and estimated block model grades showing a good correlation to one another despite the limited amount of data available.

1.6 Mineral Resource Statement

SRK has reviewed and adopted the geological models, made spot checks of the drilling database entries against assay certificates and has classified and run pit shells on the block model. SRK has then undertaken the work required to determine the reasonable prospects for eventual economic extraction, by limiting the reported tonnage to a pit shell and by applying a suitable cut-off grade of 1.3% TREO which was based on:-

- benchmarked cost parameters;
- a review of prevailing metal prices; and
- a review of E-Tech’s expectations with respect to concentrate quality and pricing discounts.

SRK has then reported a Mineral Resource statement in accordance with guidelines and terminology given in the December 2012 Australian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves prepared by the Joint Ore Reserves Committee of the Australian Institute of Mining and Metallurgy, the Australian Institute of Geoscientists and the Minerals Council of Australia (“the JORC Code”).

The JORC Code is recognized under NI 43-101 as an acceptable foreign code that governs the estimation and disclosure of Mineral Resources and Mineral Reserves. The JORC Code uses definitions and categories that are consistent with the International Reporting Template, published by the Committee for Mineral Reserves International Reporting Standards (“the CRIRSCO Template”).

The Mineral Resource statement has been prepared by Mr Martin Pittuck, CEng., MIMMM, FGS who is a Qualified Person ("QP") according to the definition of this given in NI 43-101. Mr Pittuck is a full-time employee of SRK and is independent of Battery Road, E-Tech Namibia and E-Tech Metals Ltd and their subsidiaries. The statement is effective as of 02 August 2021.

The Mineral Resource statement is given in Table 1-1 below.

Table 1-1: Eureka REE Project, Mineral Resource, August 2021

Category	Tonnage (Kt)	Grade (%TREO)	of which NdPrO*
Measured	-	-	-
Indicated	-	-	-
Inferred	310	4.8	0.7

*the sum of the individual %Nd_2O_3 and %Pr_2O_3 grades

1.7 Conclusions and Recommendations

E-Tech Namibia has undertaken exploration in a cost-effective manner, using industry standard methods and this has enabled the production of a maiden Inferred Mineral Resource estimate for the Eureka Project carbonatite dykes of 310 Kt at a mean grade of 4.8% total rare earth oxide. If only considering the Nd_2O_3 and Pr_2O_3, which are of greatest interest to E-Tech Namibia and potential offtakers, their combined grade is 0.7%.

There is significant potential to increase the size of the Mineral Resource with further exploration. Based on the radiometric anomalies and mapped outcrops yet to be tested with trenching, SRK has also therefore reported an Exploration Target of between 500 and 1,500 Kt at an average grade of between 2% and 5% TREO.

Battery Road intends to use funds raised in the RTO to accelerate work on the Project over a 14 month period. The recommended work program will cover:

- Assaying of the trench and drilling samples collected in 2020-2021;
- Diamond drilling to infill and expand coverage on the known mineralised dykes;
- Continued metallurgical testwork to improve recovery, product quality and confidence in related project cost estimates;
- Costs associated with running the exploration programme; and
- Initiation of certain studies which will contribute to a Prefeasibility Study.

Work will be undertaken in a methodical and staged manner with milestones and decision points along the way such as Mineral Resource updates and a PEA.

SRK believes there is good potential to increase the Mineral Resource on the Project through additional exploration and develop the many technical-economic aspects towards favourable outcomes. Inferred Mineral Resources have a low level of confidence by definition, and infill drilling with better quality sampling is required to increase the level of confidence and classify Indicated Mineral Resources in order to advance the Project to a Prefeasibility Study. Whilst SRK expects this to succeed, there is no guarantee that the Inferred Mineral Resources will be converted to Indicated Mineral Resources following infill drilling.

The technical-economic parameters presented in this report are mostly conceptual and they may change significantly as the work progresses to improve confidence in them. The rare earth prices are based on a 2.5 year trailing average as of June 2020 and these prices may increase or decrease in the future. The other assumptions around revenue, and price discounts in particular, are based on an understanding of what other producers in the industry are doing. E-Tech Namibia will need to develop its own arrangements in due course and these may be different for what is assumed in this ITR.

2 INTRODUCTION

2.1 Issuer and Terms of Reference

SRK Consulting (UK) Ltd. ("SRK") has been asked by Battery Road Capital Corp. ("Battery Road", the "Company" or the "Client") to review the Eureka Rare Earth Element ("REE") Project in Namibia ("Eureka" or the "Project") which is owned 100% by E-Tech Kalapuse Mining (Pty) Limited ("E-Tech Namibia") and to summarise pertinent details in an Independent Technical Report ("ITR").

The ITR will be used in support of a reverse take-over ("RTO") of E-Tech Namibia by Battery Road which is currently listed on the TSX Venture Exchange (TSXV:BTRY.P). The Transaction also contemplates a concurrent private placement by Battery Road to raise $5,000,000 on market terms.

E-Tech Namibia has an Exclusive Prospecting Licence 6762 covering the Project area which is in the Erongo Region of Namibia.

This ITR describes the work undertaken to produce a maiden Mineral Resource for the Project, and the metallurgical testwork results obtained to date as well as describing the project geology, location and ownership. The ITR also describes the merits of the project, the challenges remaining to be faced and the Company's proposed development programme.

2.2 Sources of Information

This ITR includes; a summary of exploration data collected up to August 2021, the technical work undertaken by E-Tech Metals in collaboration with Baker Geological Services Ltd ("BGS") and Impala Geomodelling Limited ("Impala") based on data collected up until May 2020, a presentation of the maiden Mineral Resource estimate for the Project and a discussion of exploration potential.

The data used for the Mineral Resource estimate, including the drillhole and trenching databases and topographic survey, was collected by E-Tech and Impala who maintained an onsite presence during the Q1 2017 drilling and the Q2 2019 trenching campaigns and assisted in collating the drillhole database, managing the exploration and Quality Assurance and Quality Control ("QA/QC") activities as well as overseeing the drilling. E-Tech also engaged the services of Mr Howard Baker (FAusIMM(CP)) of BGS to prepare a block model for the project.

2.3 Rare Earth Terminology

The Eureka deposit comprises monazite-bearing carbonatite dykes intruding quartzo-feldspathic rocks of the Etusis Formation. Rare Earth Elements ("REE") within the carbonatite dykes are exclusively contained in the monazite in which light rare earth elements ("LREE") account for 99.8% of the total REE and heavy rare earth element's ("HREE") account for the remaining 0.2%. In this report, REE may be reported as individual REE oxides ("REO") or as total rare earth oxide or ("TREO").

By virtue of the monazite concentration in the carbonatite dykes, the relative proportions of REEs in the monazite and the prevailing REE prices, Neodymium (Nd) and Praseodymium (Pr) are of key economic interest and Lanthanum (La), Cerium (Ce), Samarium (Sm), Europium (Eu) and Gadolinium (Gd) may be of lesser economic interest. The HREEs are present in trace quantities but are not currently considered to be of economic importance.

Further details are given in Section 11.9.

2.4 Site Inspections

In accordance with NI 43-101 Guidelines, Mr Keith Webb, an independent Associate Exploration Geologist with SRK, visited the Project and the sample preparation laboratory on 24th and 25th June 2020 and subsequently visited site on 26th July 2021. Mr Webb was accompanied by E-Tech Namibia's Exploration Manager, Dr Tim Smalley. Many of the outcrops, drill collars and trench locations were inspected and their locations were independently verified. The field operations office, core yard as well as the chip tray and sample storage areas were noted to be in good order.

The main purposes of the site visit were to:

- ascertain the geographical and geological setting of the Eureka deposit;
- verify the exploration work completed to date including, but not limited to:
    - confirmation of sampling and trench locations;
    - inspection of core logging and sample storage facilities;
    - review of geological interpretation and inspection of RC drill chips and core;
    - review of procedures and protocols in relation to drilling and sampling methodologies;
- assess logistical aspects and other constraints relating to the exploration property; and
- assess the overall quantity and quality of on-site work.

The most recent site visit was undertaken to confirm that there had been no material change to the scientific and technical information about the property since the personal inspection on 25th June, 2020.

Since the effective date of this report, SRK has corresponded with E-Tech Namibia and Battery Road representatives to confirm that there has been no material change to the scientific and technical information pertaining to the property and we are informed that no further assaying will be completed until the completion of the contemplated Qualifying Transaction.

3 RELIANCE ON OTHER EXPERTS

SRK has not independently verified the status or legal standing of titles and agreements relating to mineral title and ownership described in this report and relies on documentation provided by the Company.

4 PROPERTY DESCRIPTION AND LOCATION

4.1 Location

The Project is situated in the Karibib District of the Erongo Region, Namibia as shown in Figure 2-1.

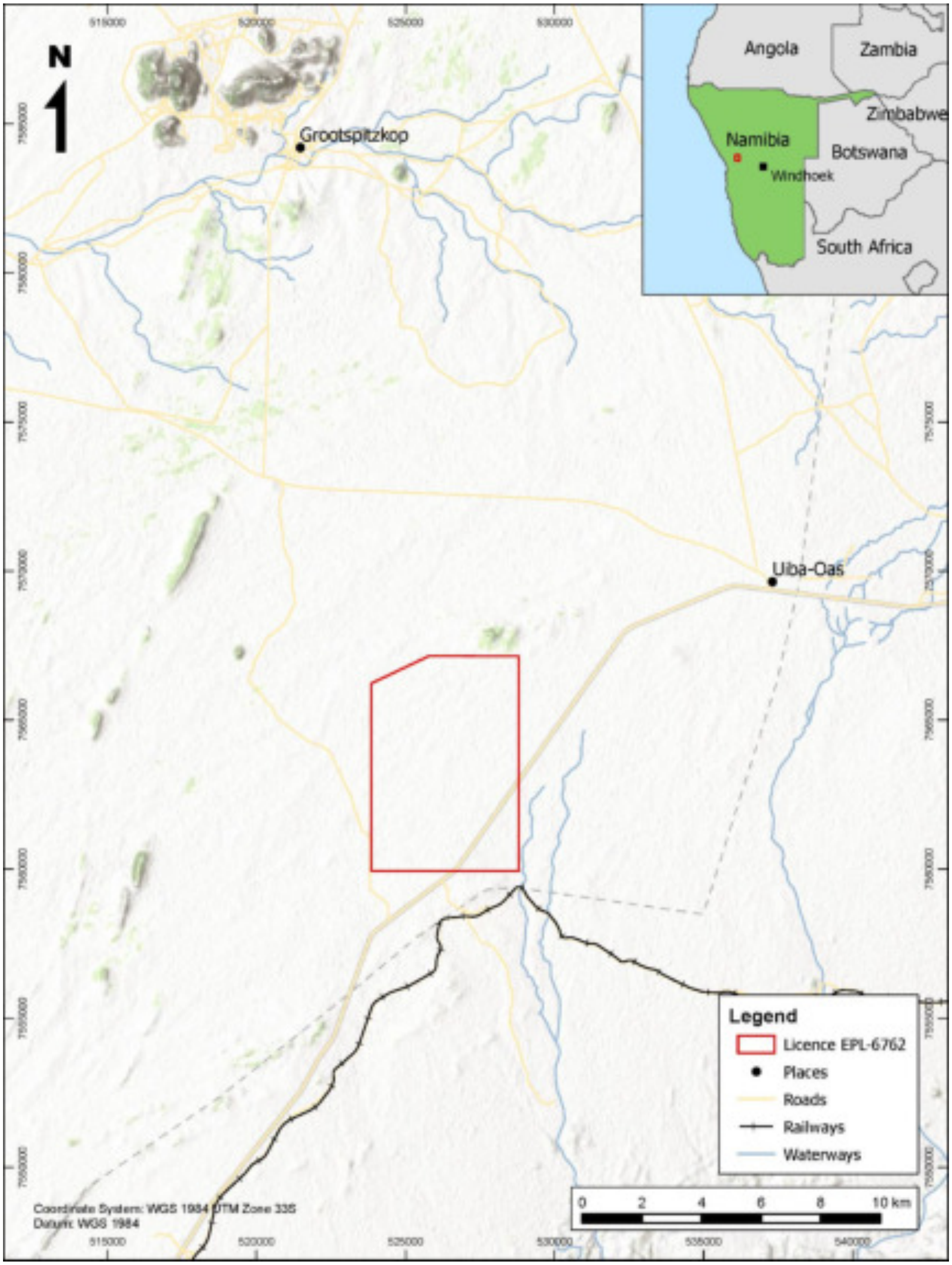

Figure 4-1: Project Location

4.2 Licence Description, Ownership and Terms

4.2.1 Licence Description and Obligations

The Eureka deposit lies within Exclusive Prospecting Licence ("EPL") 6762; which covers Eureka Farm 99 and Sukses Farm 90 and encompasses a roughly rectangular area totalling 3,474 ha. Coordinates for the EPL (both Lat-Long and WGS 84 UTM Zone 33S) are provided in Table 4-1 and shown in Figure 4-2.

Table 4-1: License coordinates for EPL-6762

POINT	LONGITUDE	LATITUDE
1	15.23110479	-22.00832942
2	15.24990324	-22.00000013
3	15.27896487	-22.00009618
4	15.27914855	-22.06510977
5	15.23121859	-22.06518448
POINT	UTM X	UTM Y
1	523851.0	7566233.1
2	525792.8	7567152.0
3	528792.6	7567136.2
4	528798.4	755939.8
5	523853.2	7559939.8

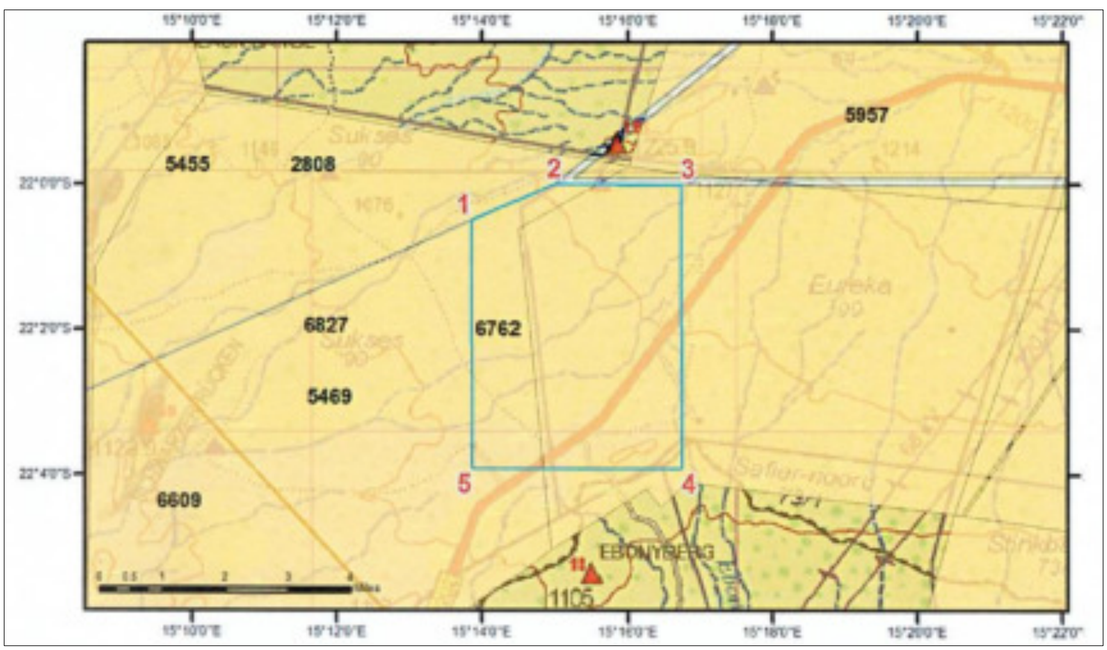

Figure 4-2 : EPL 6762 outlined in blue

The previous licence holder, KALAPUSE GENERAL DEALERS cc ("KGD") agreed to excise the Eureka licence area from its EPL 5469 licence area with the consent of Namibia's Ministry of Mines & Energy in a letter received on 15 June 2017.

EPL 6762 was then awarded to E-Tech Namibia on 12th February 2018 for an initial 3 year duration; and for the exploration of base and rare metals, industrial minerals, nuclear fuel minerals and precious metals until 12th February 2021. The licence may then be renewed for a further two periods of two years each. Additional licence renewals, beyond seven years, are possible with approval from the Minister of Mines and Energy.

E-Tech submitted their application and payment for licence renewal on 3rd November 2020, 90 days ahead of the expiry date; the licence was renewed on 20th July 2021 and is valid until 19th July 2023.

At the time KGD ceded rights to E-Tech Namibia, a non-refundable consideration of GBP 7,500 (VAT excluded) was paid by E-Tech Namibia to KGD and one half of the second non-refundable consideration of GBP 7,500 was paid in November 2020 the second half of which will be paid upon successful completion of the share exchange agreement between E-Tech Namibia shareholders and Battery Road.

Upon the successful conclusion of a prefeasibility study (“PFS”) and progression towards definitive feasibility studies and mine development, E-Tech Namibia is required to pay a further non-refundable consideration of GBP 50,000 (VAT excluded) to KGD. This has not yet been paid.

In addition, E-Tech Namibia pays under contract Early Prospecting Stage farmer compensation of NAD 2,500 per month.

4.2.2 Ownership and Transaction Details

Battery Road entered into a definitive share exchange agreement with E-Tech Namibia dated October 10, 2020 (the “Definitive Agreement”), pursuant to which the holders of all of the outstanding shares of E-Tech Namibia will exchange all such shares to Battery Road in exchange for common shares of Battery Road. After conclusion of the transaction Battery Road (the "Resulting Issuer") will be the 100% owner of all the outstanding shares of E-Tech Namibia and will continue the business of E-Tech Namibia and initially will be engaged in the exploration and development of prospective mineral properties located in Namibia, with a focus on rare earth exploration and development.

On June 2, 2021, the Corporation entered into an agreement amending its Definitive Agreement with E-Tech Namibia. Amendments included:

(i) a financing be conducted by Battery Road through the issuance of subscription receipts convertible into common shares of Battery Road, as opposed to a financing conducted by offering shares of E-Tech Namibia,

(ii) the proposed completion of a stock split by Battery Road on the basis of 2 post-split common shares of Battery Road for every 1 pre-split common share of Battery Road, and

(iii) the exchange ratio of the Definitive Agreement was adjusted for the contemplated stock split such that each ordinary share of E-Tech Namibia will convert into 111,111.2 post-split shares of the Corporation.

The amended Defintiive Agreement with E-Tech Namibia is intended to constitute the Qualifying Transaction of Battery Road, as such term is defined in Policy 2.4 of the TSX-V and will result in a reverse takeover of Battery Road wherein Battery Road will become the 100% owner of all outstanding shares of E-Tech Namibia.

To give effect to the amended Definitive Agreement, parties to the agreement will take several actions including:

- Battery Road will conduct a 2 for 1 stock split and name change;
- Battery Road will conduct a concurrent financing of subscription receipts convertible into post-split shares of the Corporation;
- Convertible debentures of E-Tech Namibia will convert into ordinary shares of E-Tech Namibia;
- The exchange of shares contemplated in the Definitive Agreement and the additional shares of E-Tech Namibia issued upon conversion of the convertible debentures of E-Tech Namibia will occur; and
- Subscription receipts from the concurrent private placement will convert into post-split shares of Battery Road.

As a result of the Qualifying Transaction Battery Road will have acquired each of the issued and outstanding E-Tech Namibia shares pursuant to the terms of the Definitive Agreement, in exchange for 111,111.2 common shares of the Resulting Issuer. Existing shareholders of E-Tech Namibia's 200 issued and outstanding E-Tech Namibia Shares are expected to receive 22,222,240 post-split common shares of the Resulting Issuer in aggregate at closing of the Qualifying Transaction. Holders of E-Tech Namibia's convertible debentures in the amount of $1,596,000 are expected to receive 133 shares of E-Tech Namibia upon conversion, which will be exchanged for 14,777,790 post- split common shares of the Resulting Issuer. It is also expected that 20,000,000 post-split common shares of the Corporation will be issued pursuant to the concurrent private placement; and, current holders of Battery Road common shares will have an aggregate of 25,971,530 post-split common shares after the Qualifying Transaction.

In association with the transaction, the obligations outlined in Sections 4.2.1 and 4.3 will also be assumed by the Resulting Issuer in respect of the Eureka project. The Resulting Issuer will assume a royalty of 1.5% of the gross value of the products sold from mining.

4.3 Surface Rights and Exploration Access

4.3.1 Permitting

An Environmental Clearance Certificate ("ECC") issued by the Ministry of Environment & Tourism, Namibia ("MET"), is the only permit required to undertake prospecting activities. An ECC was originally granted to E-Tech Namibia on behalf of KGD on 30th November 2016 and an updated ECC was granted on 3rd August 2018 which has a 3 year duration ending 2nd August 2021. An ECC renewal application was filed on 2nd June 2021 more than 60 days before the expiry date.

E-Tech Namibia has met and exceeded the obligations to keep the ECC valid and whilst no formal decision has been made in respect of the ECC renewal as of the date of this report, the Company has no reason to believe that the Minister will not grant the renewal application. Until the application is granted or refused, the ECC remains valid and in force, notwithstanding the expiry date of 2nd August 2021.

Environmental Impact Assessments and ECC's are regulated by the MET in terms of the Environmental Management Act, 7 of 2007 which was gazetted on 27th December 2007 (Government Gazette No. 3966).

The ECC application and update was undertaken by Alex Speiser Environmental Consultants ("ASEC"). ASEC undertook the Environmental Impact Assessment ("EIA") process and to compiled an Environmental Scoping Report and Management Plan for the proposed exploration activities on EPL 6762. E-Tech Namibian continues retain ASEC to carry out bi-annual environmental status reports on the EPL. The environmental aspects associated with the E-Tech Namibia's exploration activities have been successfully identified, assessed and deemed to be of very low impact as part the completed EIA Scoping report. The company continues to successfully instated relevant mitigation measures that were identified in the EMP.

No environmental liabilities have been identified by the work undertaken to date.

4.3.2 Access and Compensation Arrangements

The Project is located within state owned "Eureka Farm 99". E-Tech Namibia entered into a compensation agreement on 5th September 2016 with the state appointed farmer under Section 52 of Act No.33 of the Minerals (Prospecting and Mining) Act, 1992 which stipulates that the Prospector shall be granted access and may undertake prospecting including pitting (excluding soil sampling), trenching and drilling operations by means of percussion and/or diamond drills.

Compensation is paid according to the following terms (the NAD:CAD exchange rate is approximately 10:1)

- NAD 5,000 per month.
- NAD 500 per percussion drill hole.
- NAD 1,000 per diamond drillhole.
- NAD 5,000 per rig for each month there are more than 2 rigs drilling on the property.
- NAD 1,000 per month ground rental for a secure shipping container on site.

5 ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY

5.1 Physiography and Climate

Namibia has a warm desert to semi-arid climate with two distinct wet seasons either side of summer. Temperatures during the summer months can reach into the high 30's (°C) and during winter months temperature can be as low as 6 °C. Rainfall is extremely variable and the location can go without rainfall for numerous years.

The Project area is rocky semi-arid desert terrain located at the boundary between the Namib Desert and the Great Escarpment, vegetation in the areas is a combination of Namib grassland and sparse shrubland; some acacia trees grow in the ephemeral riverbeds on the Property. The Project area is at an elevation of approximately 1,080m above sea level, it is flat, arid and climatically stable with very low rainfall even during the rainy seasons resulting in an all-year operating season. The area lies at the eastern edge of the coastal fog zone which brings occasional costal moisture. There are many areas where site facilities and waste storage could potentially be situated.

The water table is at a depth of some 50m, this has been intersected by several reverse circulation drillholes, however the potential for this to provide sufficient water for any eventual mining and processing operations has not yet been assessed.

5.2 Project Access

Namibia is bordered by South Africa to the south, Angola to the north and Botswana to the east. In addition, Namibia shares narrow sections of border with Zambia and Zimbabwe along the Caprivi Strip and it is possible to enter Namibia by road from a number of border entry points. Namibia has a well-established road infrastructure with the majority of towns and communities accessible by a network of well-maintained gravel trunk, main and district roads totalling a distance of some 48,100 km, including 4,500 km of tarred roads.

The Trans-Kalahari and the Trans-Caprivi highways provide tarred road links between the Namibian port of Walvis Bay on the Atlantic coast, and landlocked neighbouring countries. The Trans-Kalahari highway passes within 2 km of the project site providing direct access to the capital Windhoek as well as port facilities at Walvis Bay. The Project is 250 km by road from the capital Windhoek, a journey of approximately 2.5 hours.

Namibia's railway network is managed by TransNamib Holdings Ltd. and comprises some 2,380 km of 1.067 m narrow gauge railway lines. The main line runs from the South African border at Ariamsvlei, through Windhoek and terminates at Walvis Bay, passing within 4 km of the Project site.

Namibia's main road and rail network is shown in Figure 5-1 in relation to the project location.

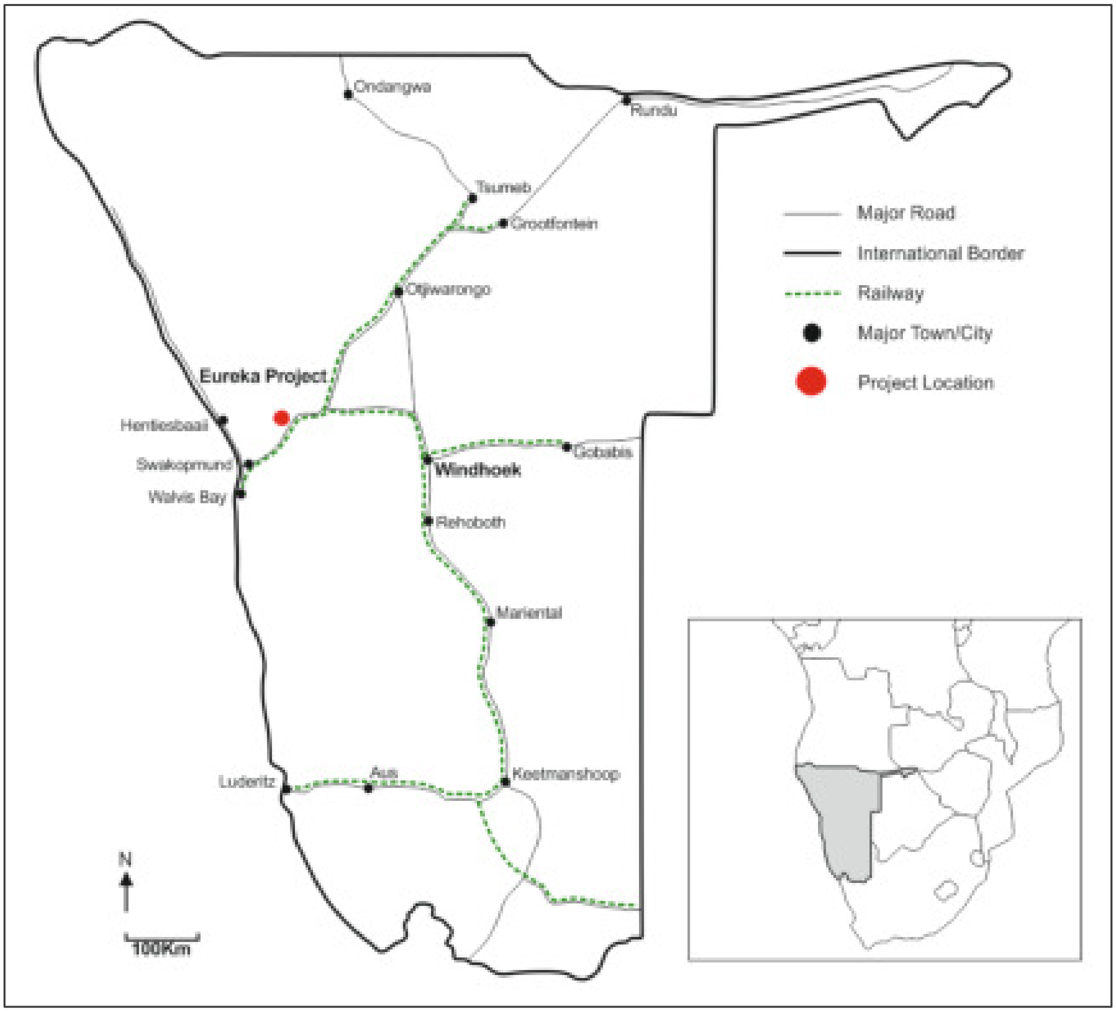

Figure 5-1: Major road and rail map of Namibia

There are direct air links to Namibia from a number of cities including Johannesburg, Cape Town, Frankfurt and Addis Ababa although flight frequency has changed recently since the national airline ceased operations. Namibia has three international airports; Hosea Kutako, Eros and Walvis Bay with Hosea Kutako airport (30 km east of Windhoek) handling the vast majority of international flights.

Walvis Bay is the main deep-water port in Namibia, with a smaller secondary port at Luderitz. The port of Walvis Bay has a depth of 12.8 m and can accommodate container vessels with a maximum capacity of 2,400 tonnes. A new cargo and container quay wall has recently been completed at Walvis Bay Harbour which is 500 m in length with a channel draft of 8.15 m, and can accommodate vessels up to 150 m in length. The majority of Namibia's exports and imports travel through Walvis Bay, typically from/to southern, western and central Africa and Europe.

5.3 Infrastructure and Local Resources

Local labour is easily sourced, either from the farms within the permit area, or from the larger towns of Usakos and Swakopmund. Namibia has a strong history of mining and exploration and skilled professionals, and drilling and exploration services, are readily available within country.

High tension, 200 kV AC, power lines run close to the Project, with a substation approximately 10 km to the south southeast. A map of local infrastructure to the project site is shown in Figure 5-2.

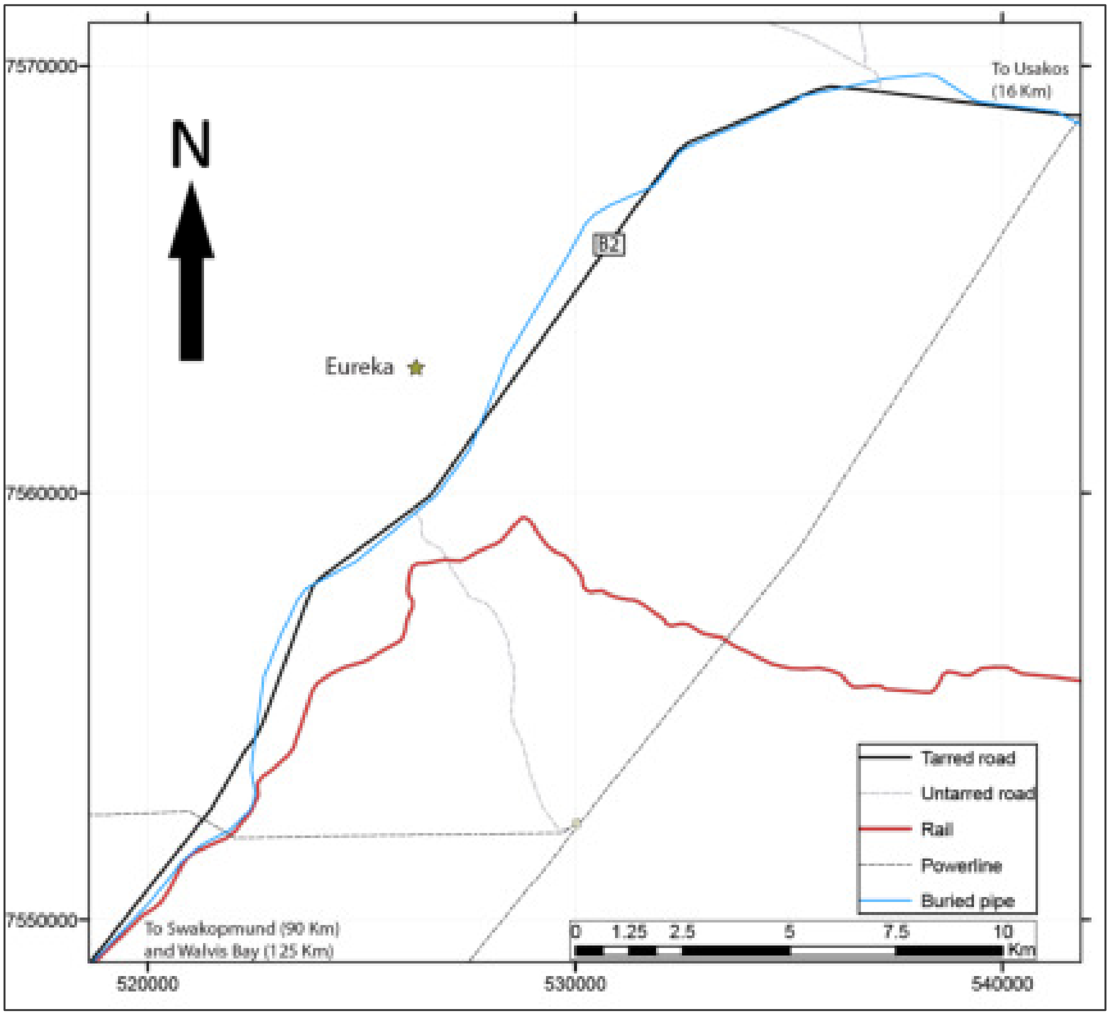

Figure 5-2: Eureka Project local infrastructure

6 HISTORY

6.1 Introduction

There is no historical Mineral Resource and there has been no historical production.

The earliest known exploration for carbonatite style REE mineralisation was conducted by Western Mining Corporation ("WMC") during the early 1980s, details of which are contained within an unpublished post-graduate thesis by Tibor Janos Dunai of Heidelberg University, Germany, completed in 1989. Subsequently the license was held by Reefton Mining and then Magna Mining, both of whom conducted exploration for tantalite pegmatite dykes. Reefton Mining identified alteration, postulated to be caused by the presence of a larger intrusive body at depth.

6.2 Surface Exploration

WMC undertook geological and radiometric mapping and identified areas of outcropping carbonatite and associated intrusive rocks; this work was compiled by E-Tech. In areas of poor outcrop, pitting was also used to assess the bedrock. In total, 8 pits were dug at Zone 1 and 2, and one at Zone 3 and some samples were taken for ore petrography. The original WMC map on the calcrete / carbonatite showing in Zone 1 is presented in Figure 6-1.

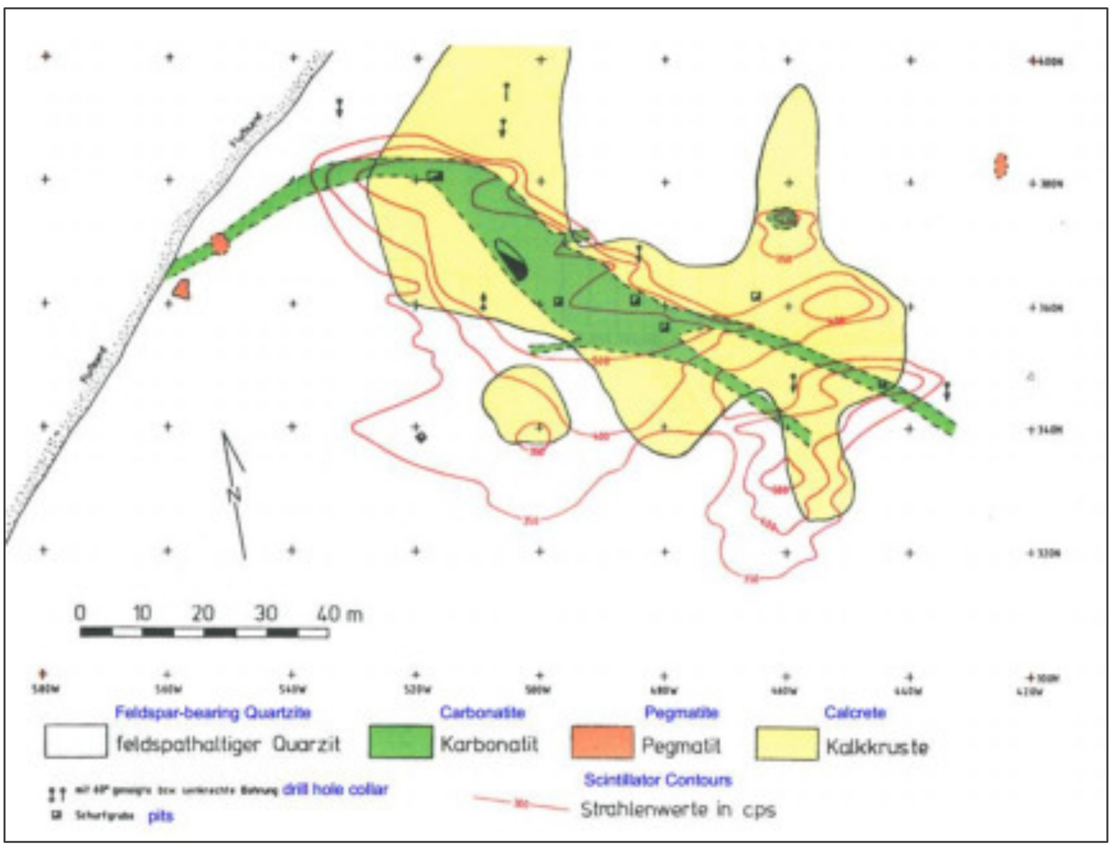

Figure 6-1: WMC Zone 1 surface geology, radiometric anomaly, pit and drillhole location map

6.3 Drilling

In 1982, WMC completed 9 small aperture percussion drillholes at Zone 1 and historical reports suggest that 7 of the drillholes intersected carbonatite. The two holes on Zone 2 drilled towards the south did not intersect carbonatite but this is unsurprising given that the dykes here are now understood to dip to the south. The 1989 Dunai report contains cross sections for 5 of the percussion holes and maps which provide some indication of hole collar locations, however, due to the uncertainty over location and assay quality, these holes have not been considered in the current study.

7 GEOLOGICAL SETTING AND MINERALISATION

7.1 Regional Geology and Tectonics

The Project is located within the Southern Central Zone of the Neoproterozoic Damara Belt (Miller 2008) which was formed as part of the Pan-African orogenic event spanning 550–495 Ma, related to the closure of the Khomas Ocean.

The Southern Central Zone comprises (in stratigraphic order):

- Two suites of granites related to the Damara Orogeny.
- Swakop Group sediments, of Neoproterozoic age, comprising mica schists and marbles.
- Nosib group sediments comprising quartzite, gneiss, mica-schist, amphibolite, calc-silicate rocks and marble.
- Abbabis Metamorphic Complex gneisses of the Kalahari Craton

The Damara Orogeny metamorphosed the Southern Central Zone sediments at high temperature but low-pressure to varying degrees, with higher metamorphic grades (close to granulite facies) attained in the west, compared with mid-amphibolite facies in the east. Estimates of the timing of peak metamorphism which may vary from place to place are in the range of 534–508 Ma (Nex et al., 2001).

Structurally, the Southern Central Zone has undergone at least three distinct deformation events, relating to the Damara Orogeny causing tight, southeast to south to southwest verging isoclinal folds and upright southeast verging folds which combine to create northeast-elongated dome structures. Eureka is located close to the core of one of these domes and also close to the intersection of the Omaruru and Welwitschia Lineaments, within the lower-most Etusis Formation of the Nosib Group as shown in Figure 7-1. These structural features often influence the location of intrusive bodies and are generally thought to influence exploration potential (Corner, 2008).

Two suites of granites occur in the Southern Central Zone, relating to partial melting of the basement gneiss and the Lower Nosib sediments. These occurred during, and after, deformation relating to the Damara Orogeny. Older (560–550 Ma), syn-tectonic, granites are less common while younger, post-tectonic (523–460 Ma (Miller 2008)) are more abundant.

7.2 Local Geology and Structure

The intrusives that host the mineralisation at Eureka have been dated as being emplaced at a similar time to the regional granites, with an emplacement age of 548 ± 4 Ma (Gonçalves et al., 2017) and are the only currently known alkaline intrusions related to the Damara Orogeny. Locally there are younger Cretaceous age northeast-striking dolerite dykes as shown in Figure 5-1, and minor dykes and pegmatites.

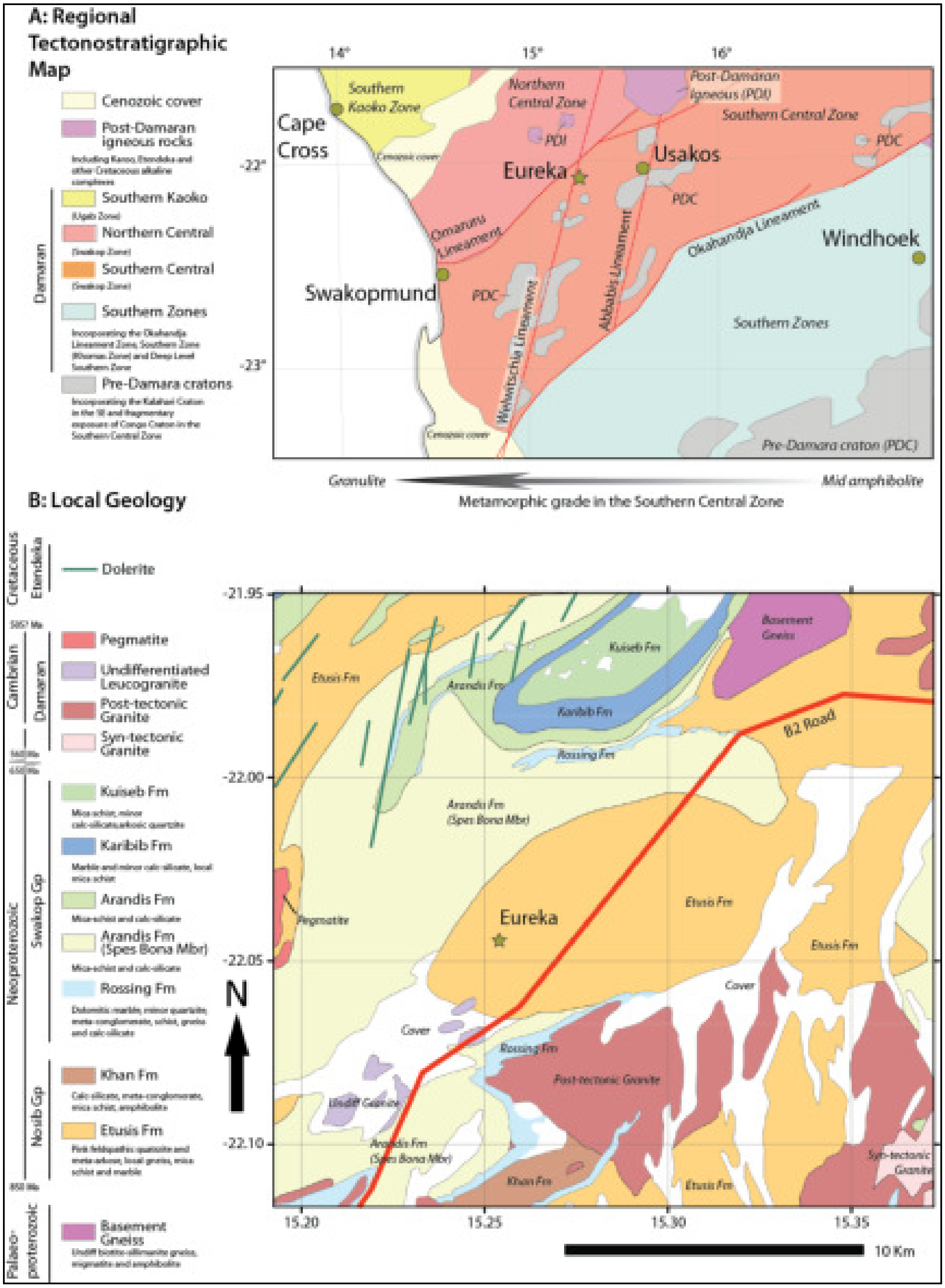

Figure 7-1: Geological context of the Project, Miller (2008) and Corner (2008)

At least 14 REE-bearing dolomite carbonatite dykes have been identified at Eureka intruding quartzo-feldspathic and calc-silicate rocks of the Etusis and Khan formations respectively. These dykes are generally greater than 0.5 m thick and there are many additional thinner veinlets of the same material. These dykes are principally composed of coarse grained (1–2 mm) dolomite, with a variable abundance of monazite (~1 mm to >7 cm grain size), magnetite, graphite, calcite, hematite and minor quartz. Locally, the dykes are surrounded by a thin selvage of skarn-like rock comprising diopside, actinolite, monazite, and graphite.

Much of the area is covered by shallow gravel and/or calcrete, consequently the dykes show as float and localised fresh or friable outcrops (e.g. Figure 7-3 and Figure 7-4) which can be detected by elevated count rates on a scintillometer.

In the trenches, carbonatite dykes are predominantly replaced by a mixture of friable secondary minerals, mainly gypsum with fluorite as well as minor calcite. Quartzo-feldspathic rocks of the basement are also weathered and show little surface expression. Calc-silicate rocks, however, are typically fresh and frequently outcrop.

Limited structural measurements on basement rocks have indicated that the first deformation stage evident at Eureka is an antiform, plunging to the north coupled with a parallel synform. A second stage fold is inferred along an ENE-WSW strike line, refolding the pre-existing antiform. Carbonatite emplacement is locally parallel to these structural trends typically following pre-existing calc-silicate units. However, thin splays of carbonatite, cross-cutting Etusis Formation rocks (Figure 7-5), demonstrate that the carbonatite dykes post-date the host rock deformation.

Figure 7-2: Monazite grains (orange) in a dolomite matrix (dark brown)

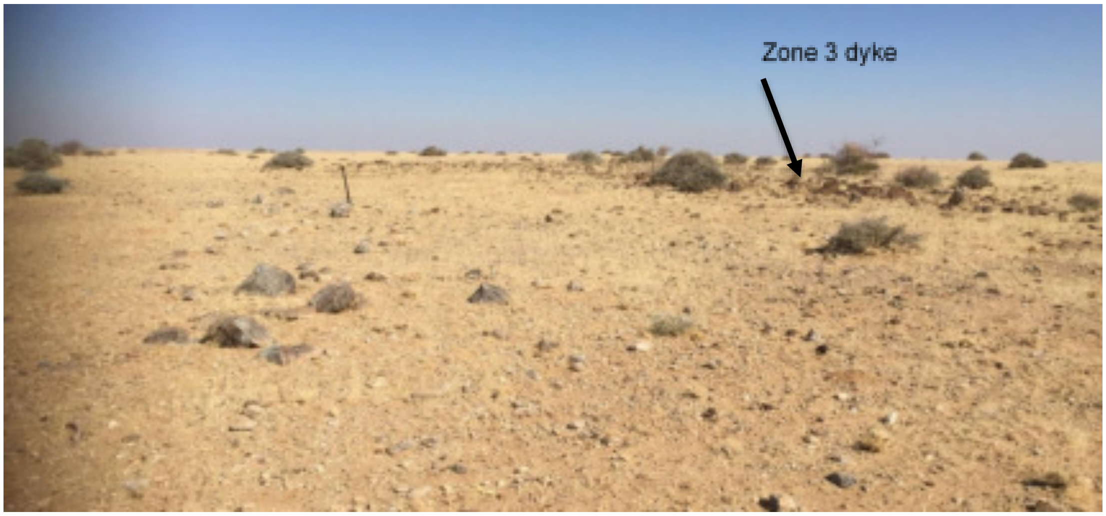

Figure 7-3: Example of exposed dyke from Zone 3

Figure 7-4: Trench cutting of weathered carbonatite

7.3 Mineralisation

7.3.1 Introduction

Mineralised dykes and veins occur in four areas termed 'Zones 1–4'. Zones 1 and 2 probably contain the same dykes whose outcrops are separated by a dry river bed. Zone 3 occurs some 250 m south of Zones 1 and 2, and Zone 4 is located approximately 500 m south of Zone 3. Figure 7-5 shows the location of carbonatite dykes (purple lines), outcrop (purple circles) and trenches; green and cream dots indicate exposure of calc-silicate rocks and Etusis Formation rocks, respectively. The colour overlay represents the results of a radiometric survey.

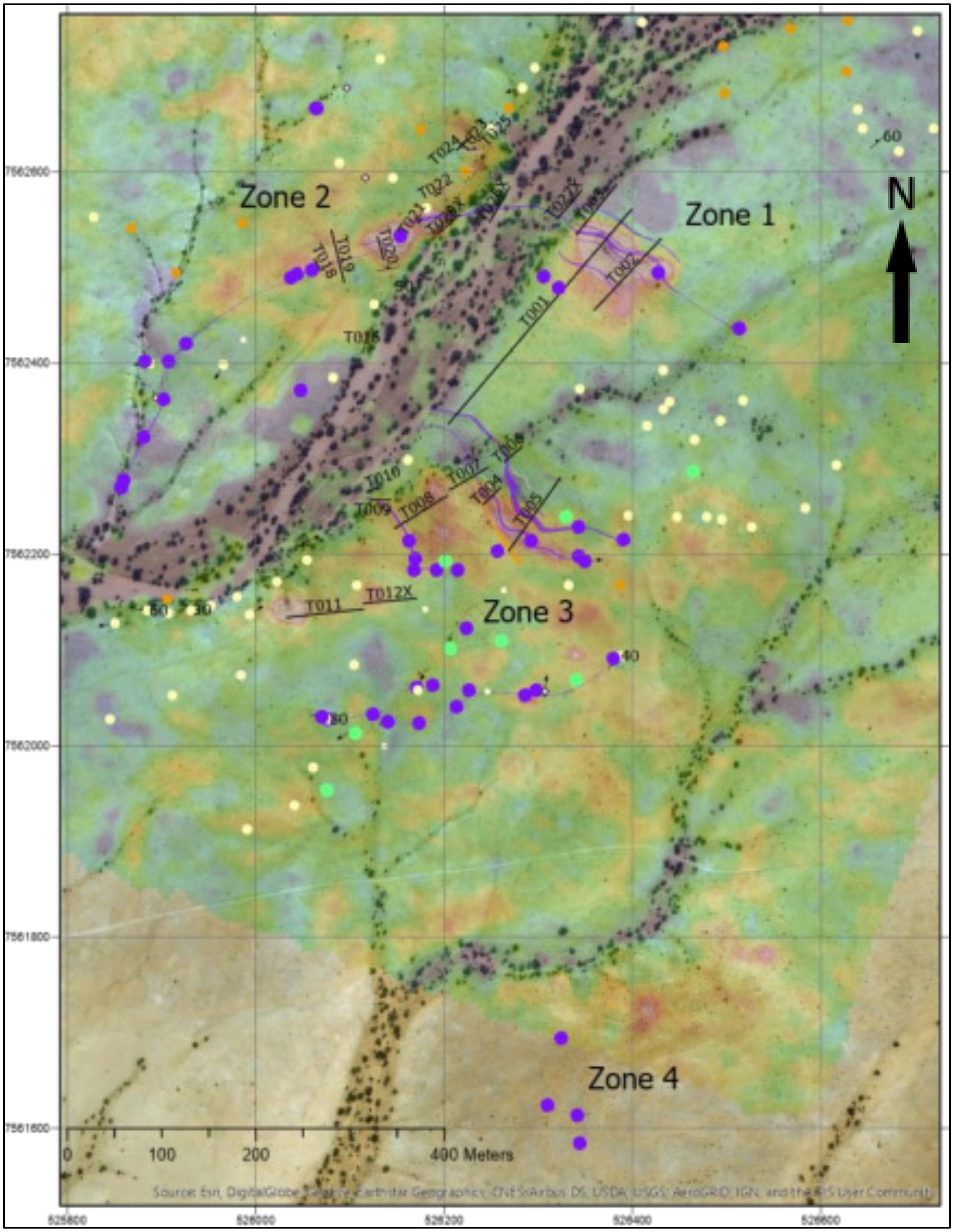

Figure 7-5: 1:5000 map of Zones 1–4

7.3.2 Zones 1 and 2

Zone 1 contains three major mineralised dykes, locally connected by at least three thinner veins. At Zone 2, trenching was less extensive, but at least three individual dykes occur. Two are 10 m apart, while a third occurs approximately 30 m further north. Trenches and limited drilling data from the dry riverbed between Zones 1 and 2 suggest that the dykes in each zone are connected along strike as shown in Figure 7-6. More trenching and/or drilling is required in this area to confirm the geometry of the dykes. Mineralised outcrop continues some 300 m SW of Trench T018 in Zone 2. A single occurrence of carbonatite outcrop occurs approximately 100 m SE of Trench 002 in Zone 1, these extensions are shown in Figure 7-5.

The true thickness of the dykes in Zones 1 and 2 varies between 0.5 and 4 m. At Zone 1, drilling intercepts indicate the dykes dip at 75° to the north. At Zone 2, drilling intercepts indicate the dyke dips at 75° to the south.

Carbonatite from Zone 1 is relatively fresh, brown/ dark brown in colour and is of medium grain size. It is rich in monazite, with the largest grains reaching up to 30 cm but most, on average, are around 1–2 cm (Figure 7-2). Carbonatite from Zone 2 is substantially more weathered than the other zones, it contains monazite and is lower grade than Zone 1. On the weathered surface, the carbonate groundmass has been replaced by chalcedony.

7.3.3 Zone 3

Zone 3 occurs approximately 250 m south of Zones 1 and 2. At least five carbonatite dykes have been identified in outcrop and trenches (Figure 7-7) in Zone 3, as well as some additional thinner carbonatite veins. Approximately 100 m to the south of the trenches a series of E-W striking mineralised carbonatite outcrops, shown in Figure 7-5., represent additional exploration potential.

Mineralisation in Zone 3 is less uniform than in Zones 1 and 2. The central dyke is monazite-bearing over a distance of 75 m, the other dykes are also mineralised to a lesser extent. The monazite-bearing dyke is approximately 2.5 m thick and dips 75° to the southwest. Pegmatite dykes also occur in Zone 3, aligned approximately NW-SE. These are inferred to cross-cut carbonatite between trenches, as evidenced by a single example in outcrop.

7.3.4 Zone 4

Zone 4 is located approximately 500 m south of Zone 3 (Figure 7-5). It comprises an area of carbonatite outcrop with associated high scintillometer count rates, offering considerable exploration potential. At present, however, only limited trenching has taken place in Zone 4 but samples will not be assayed until further funds are raised and the Qualifying Transaction is completed.

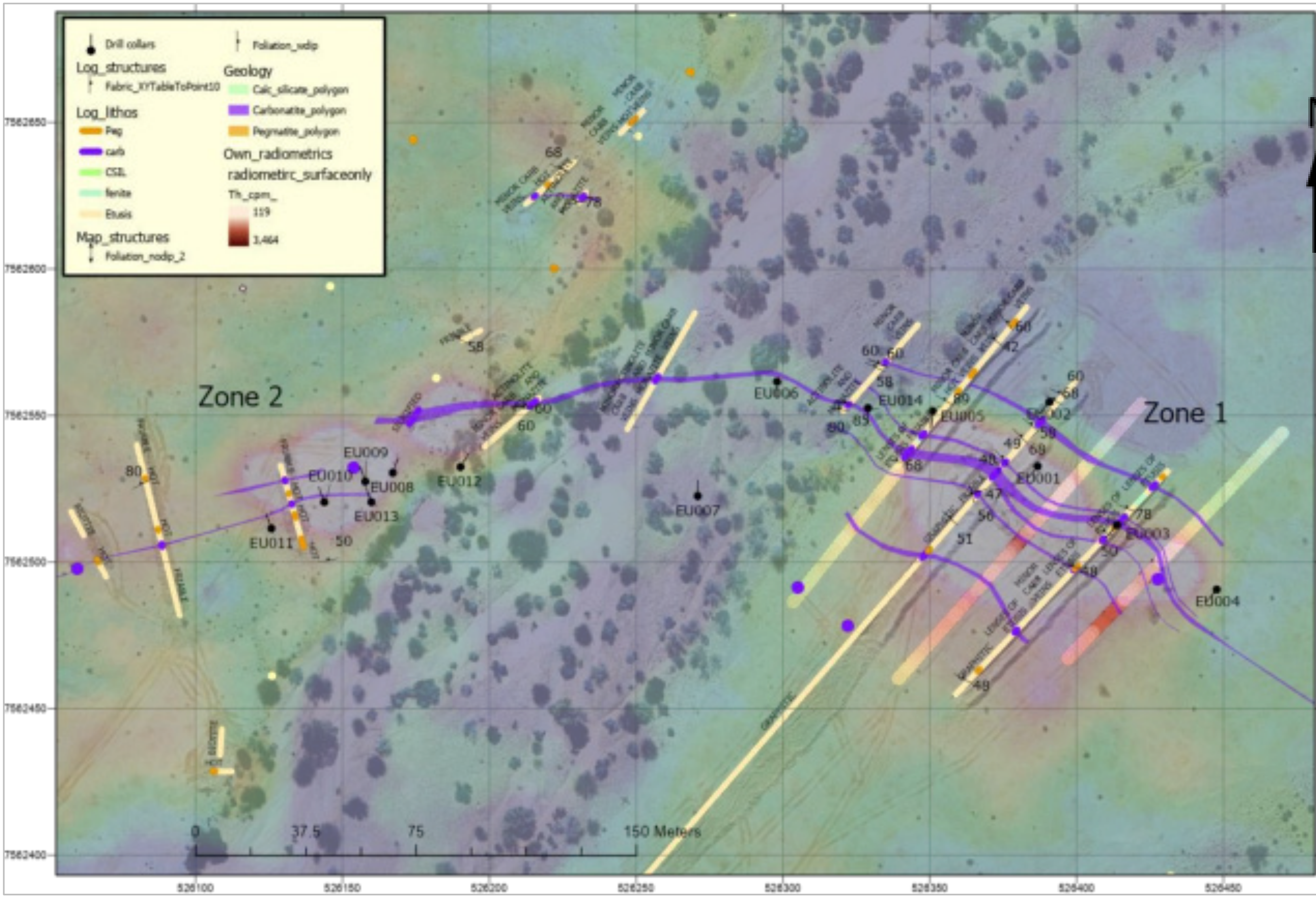

Figure 7-6: 1:1500 map Zones 1 and 2

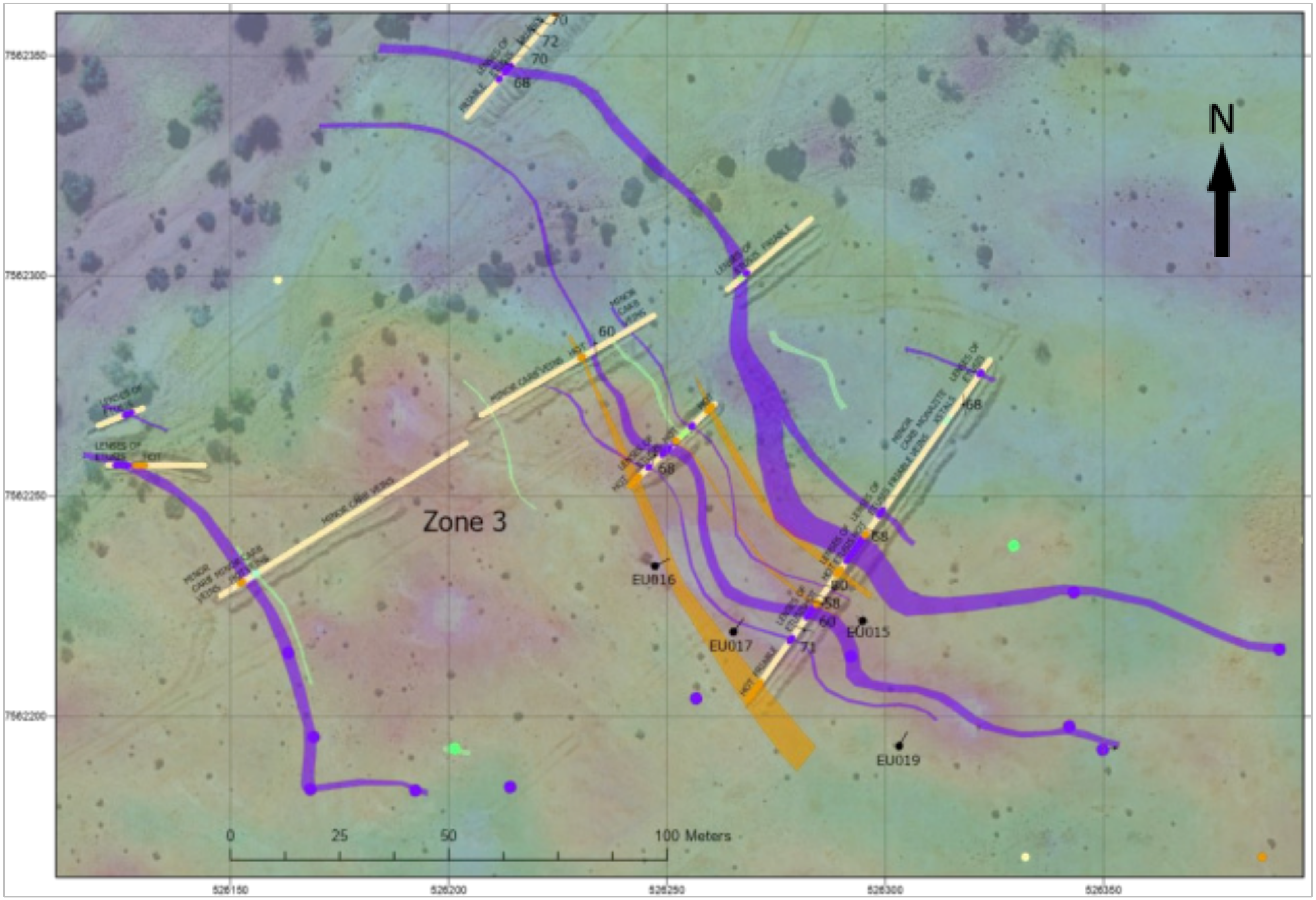

Figure 7-7: 1:1000 map of trenches at Zone 3

8 DEPOSIT TYPES

Geometrically, carbonatites are normally diatremes and poly-phase vent breccias from which dykes emanate typically covering an area measuring hundreds of metres. These bodies often cause fenitic metasomatism, chemically altering host rock minerals to alkali, ferromagnesian, sub-aluminous minerals.

Carbonatites are a mineralogically distinct family of igneous intrusion often associated with or an integral part of alkaline igneous complexes. They are depleted in silica and alumina and dominated by calcite and or dolomite. Carbonatites normally contain alkali and ferro-magnesian minerals and often contain unusual minerals hosting incompatible elements; they concentrate rare earth elements more effectively than most other rock types.

Most hard-rock commercial production of rare earth minerals is associated with carbonatites, notably the globally significant Bayan Obo mine in Inner Mongolia, the Mountain Pass mine in the USA and the Mt Weld mine in Australia.

The geometry and mineralogy of the Eureka dykes are in keeping with the characteristics associated with carbonatites globally but it remains to be seen how extensive these dykes are and whether or not they are associated with a larger body potentially near surface.

9 EXPLORATION

9.1 Introduction

This section describes the exploration data collected for the Project by E-Tech Namibia between January 2017 and August 2021.

E-Tech Namibia has been able to ground truth earlier work and to build on this with more detailed mapping, trenching and drilling. The geometry of the carbonatite dykes is now well established in many areas which have also been sampled to inform the Mineral Resource model whilst other areas have outcrop or radiometric anomalies which have yet to be followed up.

9.2 Mapping

E-Tech Namibia’s mapping was conducted in parallel with a 1.2 km trenching programme (Q2, 2019), centred on mineralisation at Zone 1 as denoted by the dashed black line in Figure 9-1. The weathering and poor exposure limits the effectiveness of mapping but when combined with the trenching, geophysical data, and radiometric data, the intermittent outcrops can be pieced together with some confidence.

Outcrop locations were recorded using a Garmin GPSMAP 66s, accurate to ± 3 m. Structural measurements were collected, with true north corrected from magnetic north by -11.5°. Structural measurements are predominantly limited to foliation in the Etusis Formation and the orientation of pegmatite dykes and quartz veins.

Polished thin sections of representative samples of all rock types, with the exception of pegmatites, were prepared in order to confirm field mineral identification and rock type.

9.3 Geophysics

In September 2016, E-Tech Namibia commissioned Gregory Symons Geophysical Services, Namibia to undertake a ground magnetic and radiometric survey over a 1.2 km² grid to improve the response and resolution previously available from the Namibian government airborne data. Surveys were performed over the Eureka carbonatite at 25 m spaced lines on a grid trending 020°. A map showing the location of the survey lines in presented in Figure 9-2.

The aim of the survey was to detect carbonatite dykes in outcrop and under shallow calcrete cover. Like most carbonatites, Eureka contains accessory magnetite easily identified by magnetic geophysical surveys. The monazite also contains an average of ~0.6 wt.% thorium which can be identified at short distances by gamma detectors; thorium levels at Eureka are too low to be detected by airborne radiometrics but are easily resolved in the ground survey.

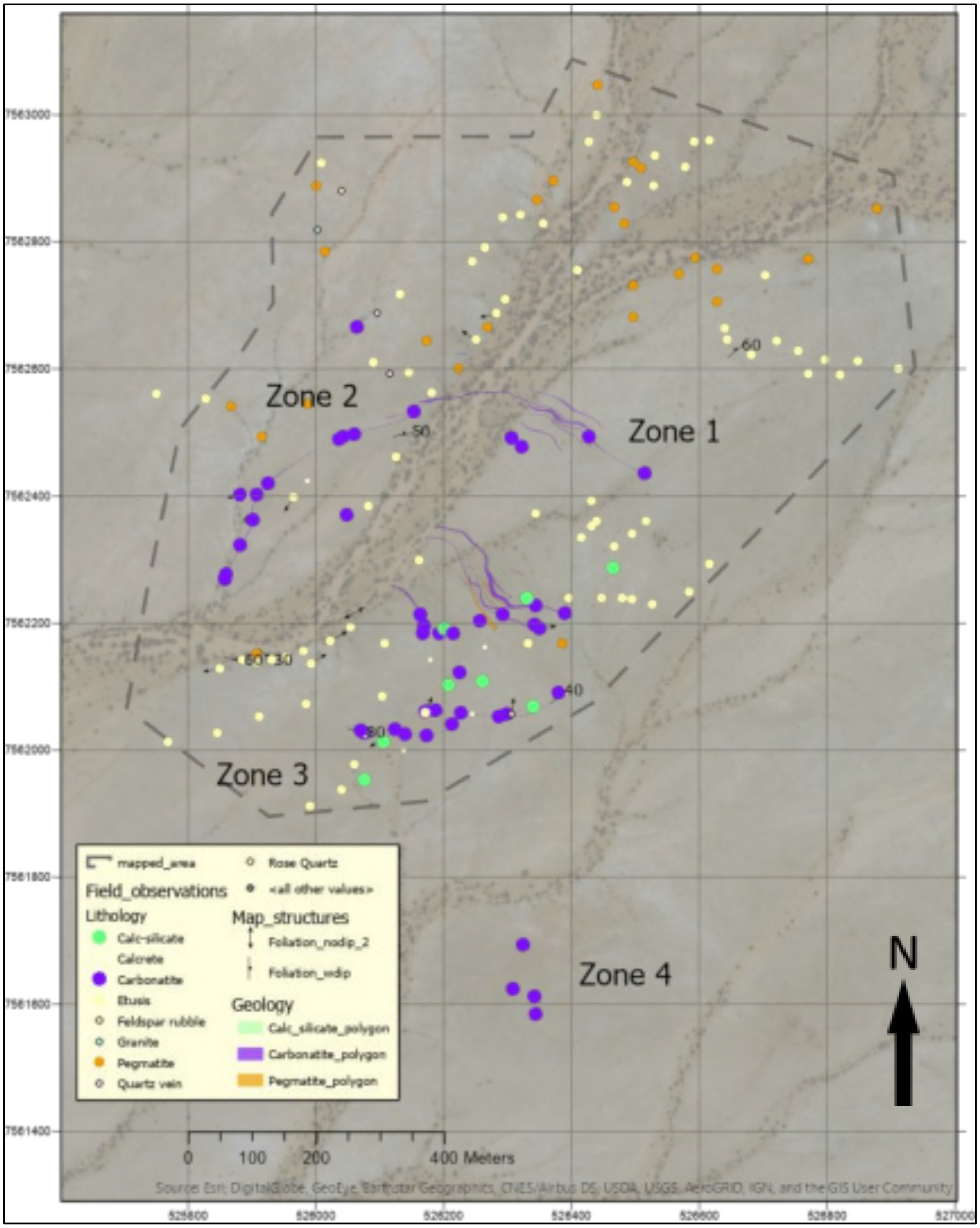

Figure 9-1: Extent of E-Tech Namibia's mapping at Eureka

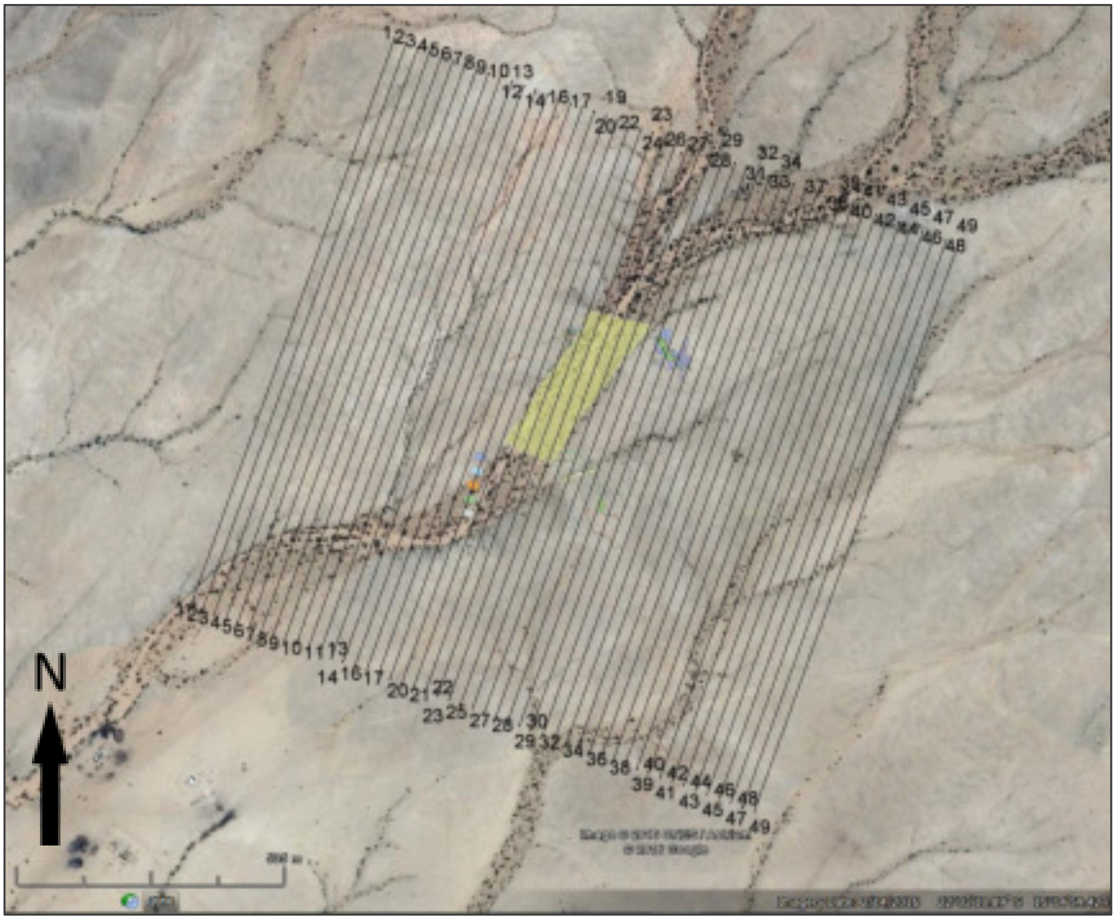

Figure 9-2: Postion of the geophysical grid

The survey utilised the following equipment:

- GEM GSM 19 Overhauser walk magnetometer.
- GEM GSM 19 Overhauser base station.
- Pico Envirotech walk Spectrometer

The survey was undertaken by Mr Willy Nuuyandja while processing, interpretation and quality control checks were undertaken by Mr Gregory Symons.

The following processing was applied to the raw magnetic data using Geosoft software:

- Diurnal Correction
- Removal of any spikes and smoothing
- Levelling

The raw data was then gridded using kriging and processed to produce Analytic Signal (AS), Reduction to Pole (RTP) Tilt Derivative (TDR), Horizontal Gradient Tilt Derivatives and Vertical Derivatives (VD) files.

Spectral Stripping of data from counts per second ("CPS") to equivalent elemental grades (ppm) and dose was then undertaken using Geosoft and once this processing was completed, the data was gridded and images showing CPS and equivalent elemental data were produced.

The image shown in Figure 9-3 is a compilation and interpretation of several layers of geophysical results from the Greg Symons report with an overlay of trench and RC drillhole collar positions representing the data used in the MRE.

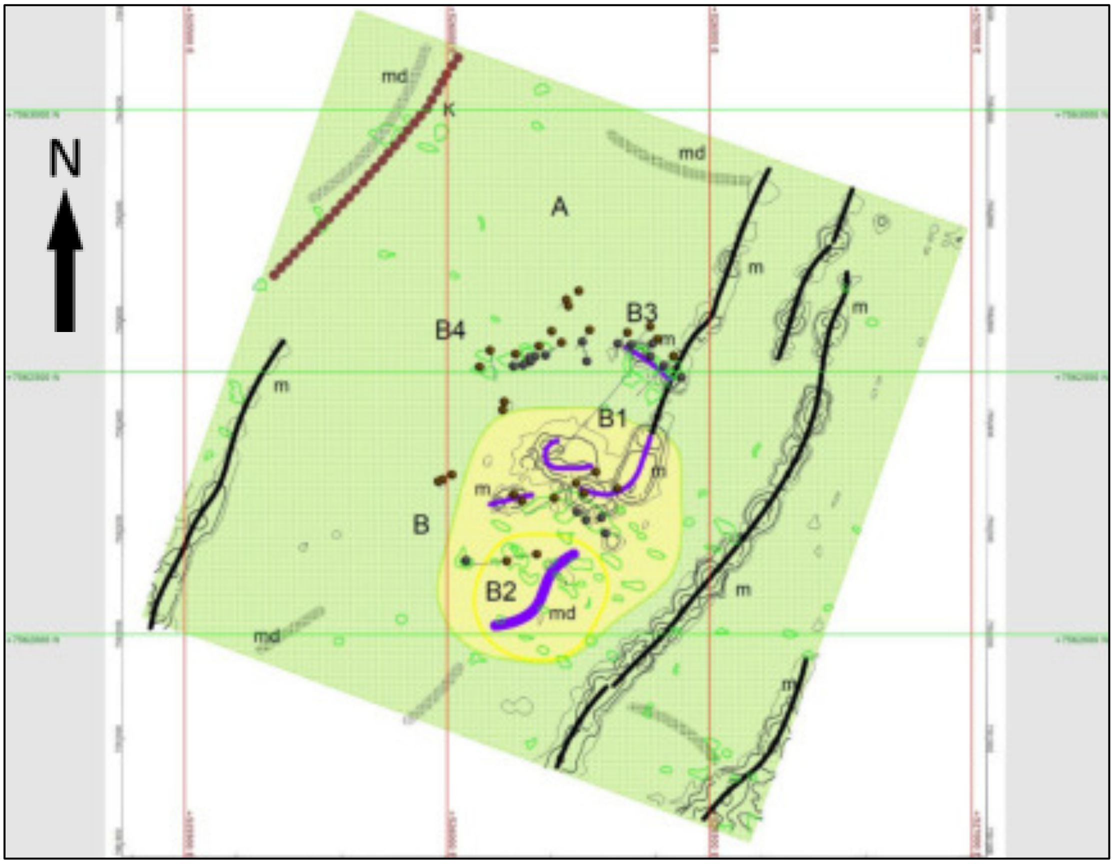

Figure 9-3: Geophysics Interpretation

Notable features are:

- a number of NNE-striking magnetic highs shown as thick black lines interpreted to represent dolerite dykes;
- thin black contour lines representing magnetic highs associated with dolerite dykes and shallow magnetite-bearing carbonatite dykes further highlighted with thin purple lines;
- thin green contour lines representing high thorium count features interpreted to be shallow monazite-bearing carbonatite dykes;
- Yellow filled area labelled B1-B2 (representing Zone 3) interpreted to represent a magnetic carbonatite stock near surface at B1 represented by thin purple lines and deeper below surface at B2 represented by the thick purple line;
- B4-B3 features (referred to as Zone 2 and Zone 1) representing high magnetic and thorium responses interpreted to represent a possible ring dyke feature arranged concentrically around the stock; and
- an area with more frequent high thorium responses centred on the B2 area interpreted to be associated with monazite-bearing features.

9.4 Trenching

9.4.1 Planning and Surveying

In Q2 2019 E-Tech Namibia undertook a 1.2 km trenching programme. The aim was to follow up on new targets generated from the 2017 drilling campaign, explore previously un-investigated radiometric anomalies, and to improve the mapping of the deposit. Trenches were dug to competent bedrock at a depth of 0.5–3 m.

The trenches were variably spaced, depending on the position of existing drill holes, surface outcrop and radiometric anomalies. The locations of the trenches are shown in Figure 9-4.

As of Q1 2020, Trenches T002, T003 and the northern part of Trench T001 remain open and are fenced-off; other trenches have been logged, sampled and in-filled for safety purposes.

Trench locations were initially marked with a handheld GPS and then located more precisely to match the high-resolution aerial imagery described in Section 9.4.5.

9.4.2 Logging

Logging of the trenches was undertaken soon after excavation; each metre was logged for rock type and tested with dilute hydrochloric acid to help identify carbonate bearing lithologies. Structural measurements were taken on exposed foliation, fold hinges, and lithological contacts, where these were evident.

The lithological, CPS and structural data was digitally captured and stored in a custom database.

9.4.3 Sampling

Chip samples were collected along the entire length of each trench by channel sampling in one-metre intervals along the base of the western trench wall at a constant elevation above trench base. Each sample approximated 3-4 kg of material. Samples were bagged with a unique sample ID ticket, referenced to a sample ticket book and submitted for analysis

9.4.4 Scintillometer measurements

CPS measurements were taken for each metre using a “ThermoScientific Rad Eye PRD” device. In addition, for trenches 1–3, gamma ray spectra were obtained every 2 m using a “Georadis GT-32” gamma ray spectrometer. This instrument is capable of differentiating the source of ionising radiation and the results demonstrate that elevated CPS is caused almost-exclusively by thorium which is associated with monazite and therefore correlates with TREO grade.

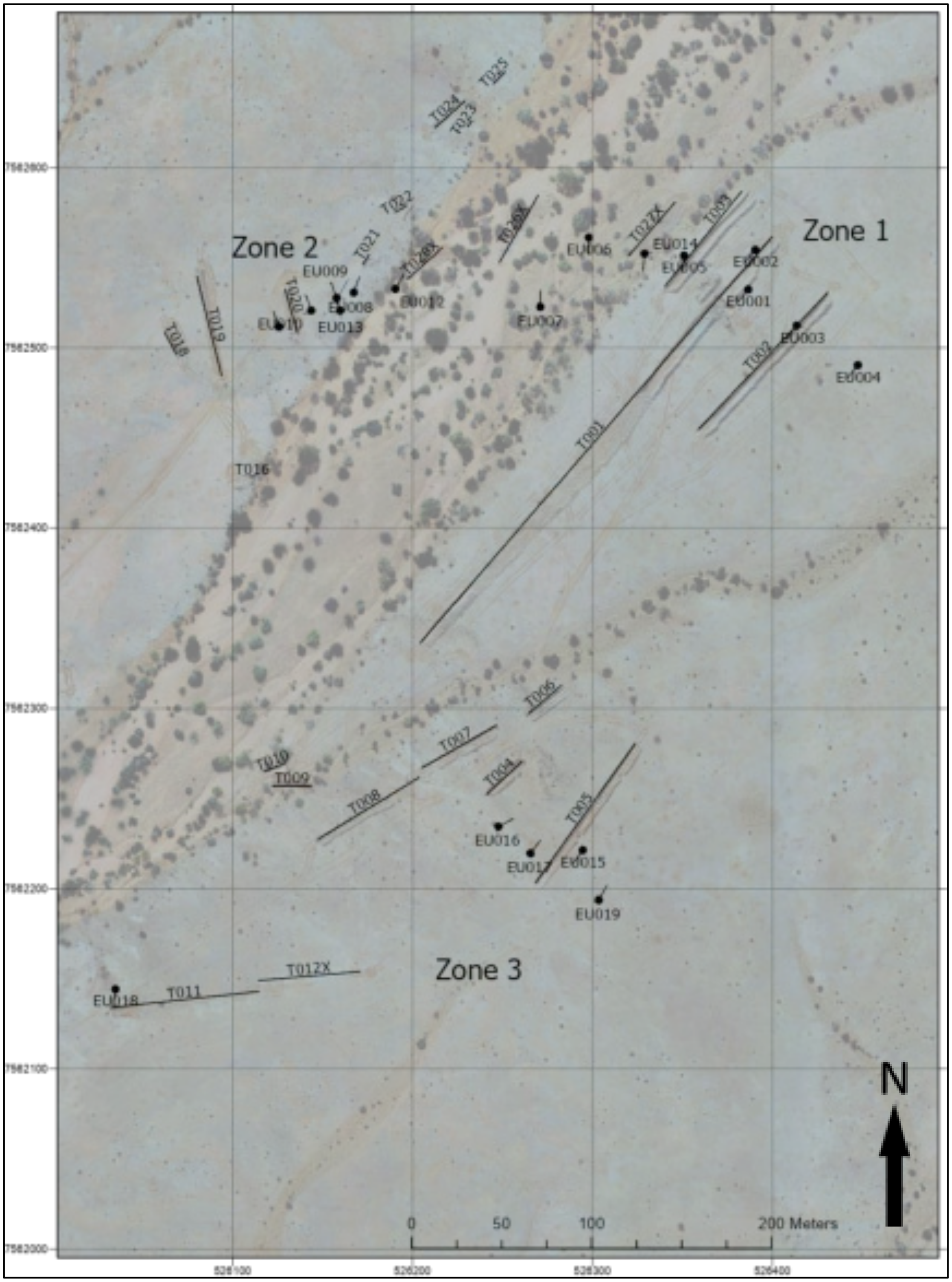

Figure 9-4: Location of trenches and drillhole collars at Eureka

9.4.5 2020 Trenching

A second trenching programme commenced in November 2020; 17 trenches were completed covering a total of 2.45 km; the first of these being TR030. Trenches were logged with a Rad Eye and the resultant CPR readings have been plotted; samples have been taken but these will not be submitted for assay until additional funds are in place. It is envisioned that only selective trench samples will be submitted, this selective submission will be guided by the Rad Eye readings.

The trenches tested the eastern part of Zone 1 where the current resource model is expected to continue along strike in a south easterly direction; and they extended to the southwest of this area where a number of new drilling targets have been delineated by high Rad Eye readings. Figure 9-5 shows the new and old trenches in Zone 1 with respect to the current resource model expression at surface.

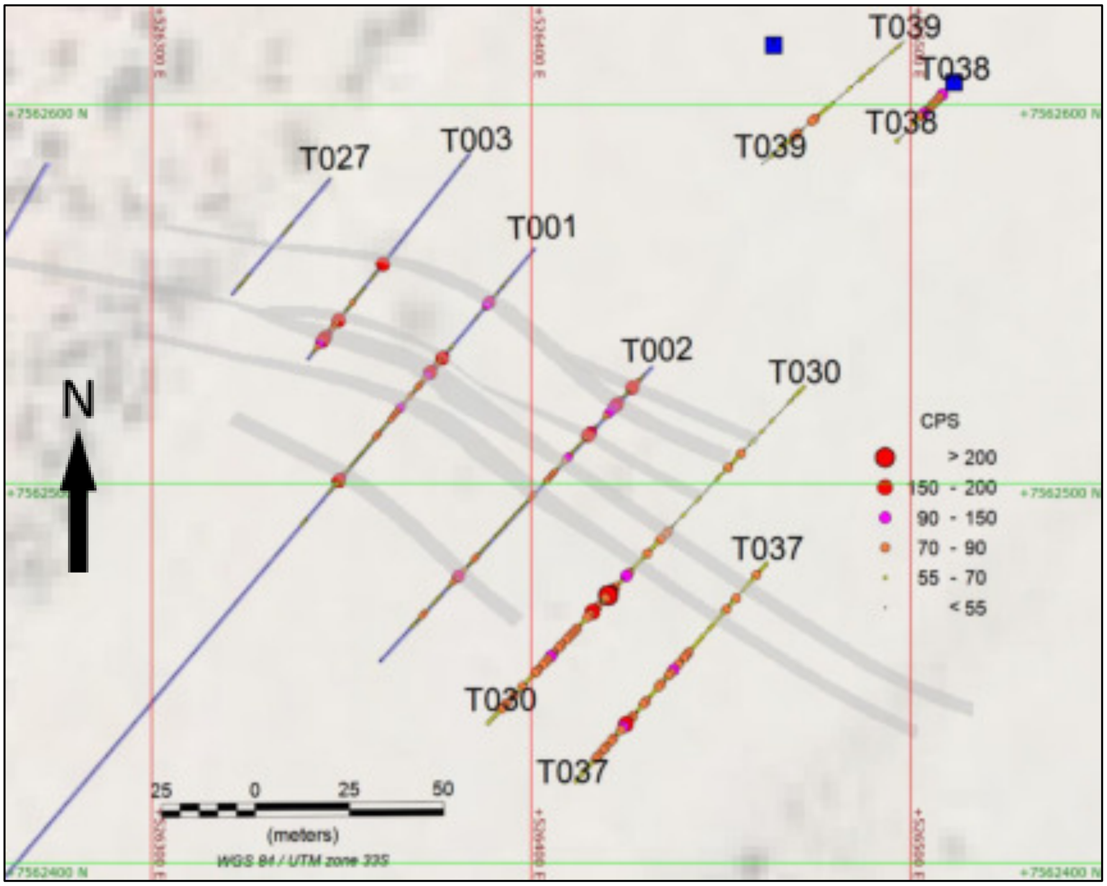

Figure 9-5: Location of new and old trenches in Zone 1

Most of the new trenches provide more comprehensive coverage at Zone 3 and extend the trenched area to the south and east. A number of new drilling targets have resulted from several southeast-trending Rad Eye anomalies which tie-in to some extent with newly mapped dyke outcrops. Figure 9-6 shows the new and old trenches in Zone 3 with respect to the current resource model expression at surface; newly mapped dyke outcrops are shown as blue square symbols.

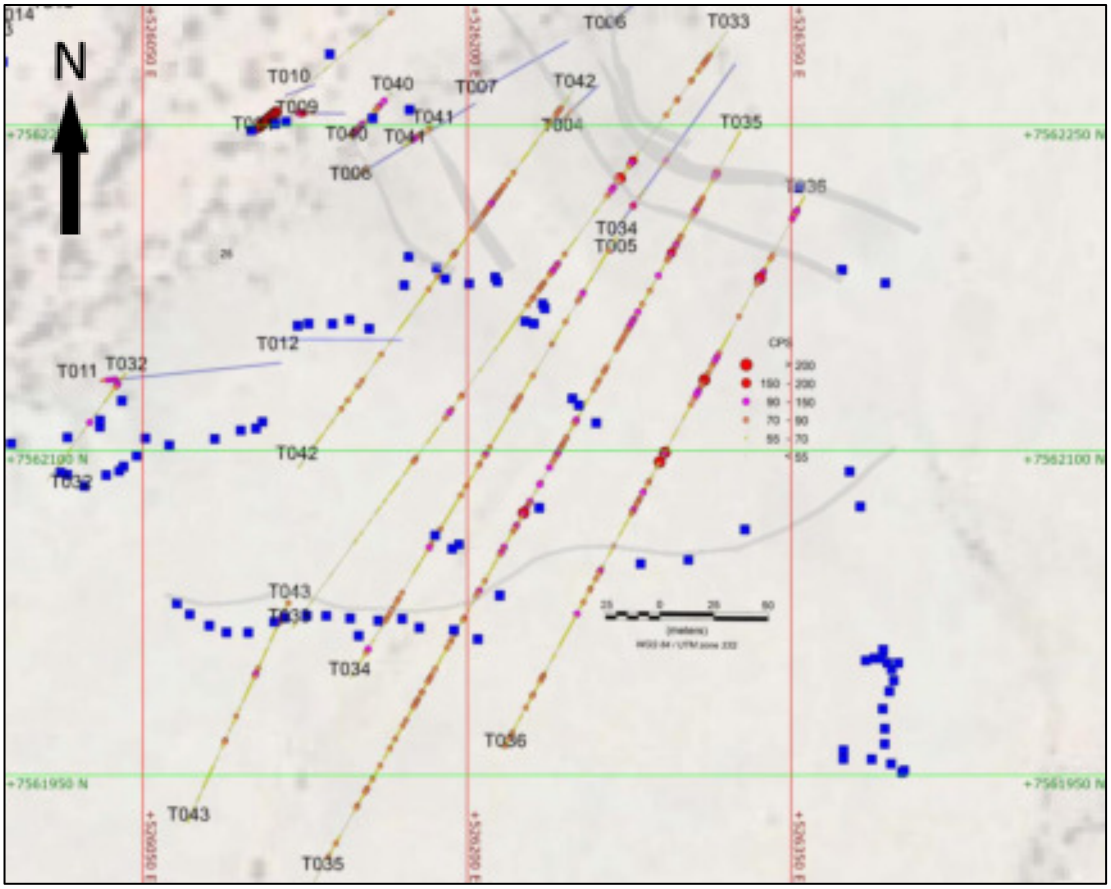

Figure 9-6: Location of new and old trenches in Zone 3

Four trenches were cut in Zone 4; the Rad Eye results from these along with newly mapped dyke outcrops show that similar mineralisation is present although widths and grades may be less than what has been encountered in Zones 1 and 3.

All trenches have been backfilled and rehabilitated to the satisfaction of the ASEC's Biannual Environmental Audit dated December 2020.

The November 2020 trench results have not been used to influence the Mineral Resource model in this report.

9.5 Aerial Photogrammetry Survey

A 1.5 km x 1 km drone mounted aerial photogrammetry survey was completed in 2019 after trenching was completed, centred over Zones 1, 2 and 3. The aerial survey produced a topographic surface for the project area with an average resolution of 0.1 m. The survey was anchored and georeferenced using the drillhole collars coordinates determined by DGPS.

9.6 E-Tech Namibia Spend to Date

A summary of E-Tech Namibia's approximate total spend on the licence to date is provided in Table 9-1 below.

Table 9-1: Summary of expenditure on the Eureka project to date

Category	Amount Spent (CAD)
Transport & Accommodation	105,700
Environmental Assessment	33,500
Geophysical Surveys	34,000
Drilling and Trenching	1,284,000
Assaying	69,500
Storage	29,300
Metallurgical Test Work	24,000
Consultancy & Salaries	289,000
TOTAL	**1,869,000**

10 DRILLING

10.1 RC Drilling for the MRE

In March 2017, a number of positive geophysical anomalies and areas with outcropping mineralisation were tested with a 19 hole RC drilling campaign (totalling 610 m). Drilling was undertaken by Hammerstein Mining & Drilling cc. using a conventional RC rig with onboard compressor. Drilling used a 133 mm diameter hammer; a sample was collected from each drilled metre using a labelled woven sack before splitting. Holes were cased using steel casing to solid ground (typically 3 m), sufficient casing was left above ground to allow the collar ID, depth, azimuth and end of hole depth to be welded to the casing to permit easy identification of holes in the field. A photograph of the drilling and sample collection in progress is provided in Figure 10-1.

A variable drill spacing was used during the drilling campaign based on the scale and complexity of surface outcrop for each zone. An approximate 30 m spacing was used for Zone 1, 15 m for Zone 2 and 25 m for Zone 3. A plan map of drillhole locations, zones and outcropping mineralisation is provided in Figure 10-2.

Collars were initially located using a handheld Garmin 62s GPS, and subsequently captured by Differential GPS ("DGPS") with a positional accuracy of <20 cm.

10.2 Logging

RC chips collected from each metre were logged for major rock type. In addition, scintillometer counts per second were recorded for each metre using a "ThermoScientific Rad Eye PRD" device to identify elevated radiation levels associated with carbonatite intervals. Each metre was also tested for reaction to dilute hydrochloric acid to help identify carbonate bearing lithologies. The weight of each sample sack was also recorded to monitor recoveries. A sample of the dust and washed chips for each metre were laid out into a chip pad and photographed, an example chip pad is shown in Figure 10-3. The lithological, CPS and recovery data was digitally captured and stored in a custom database.

10.3 Downhole Surveys

Immediately after the completion of the RC drill programme, down hole deviation, optical scanner and spectral gamma logging of all holes was completed by Terratec Geophysical Services. A downhole optical scan and spectral gamma plot through a typical mineralised horizon is presented in Figure 10-4.These logs have been integral in helping E-Tech Namibia map the mineralised dykes as well as providing information about the nature of contacts and orientation of structures. The dykes give an increased gamma response above the relatively stable background signal and often have a subtle brown/orange appearance.

The continuous downhole deviation survey, in conjunction with the DGPS unit used to locate the drillhole collars, provides an accurate 3D position for the drillhole sample locations. The deviation data captured in the first 5 m of each hole has been disregarded due to the impact of the steel casing on the magnetic field readings.

Figure 10-1: RC drilling and sample capture

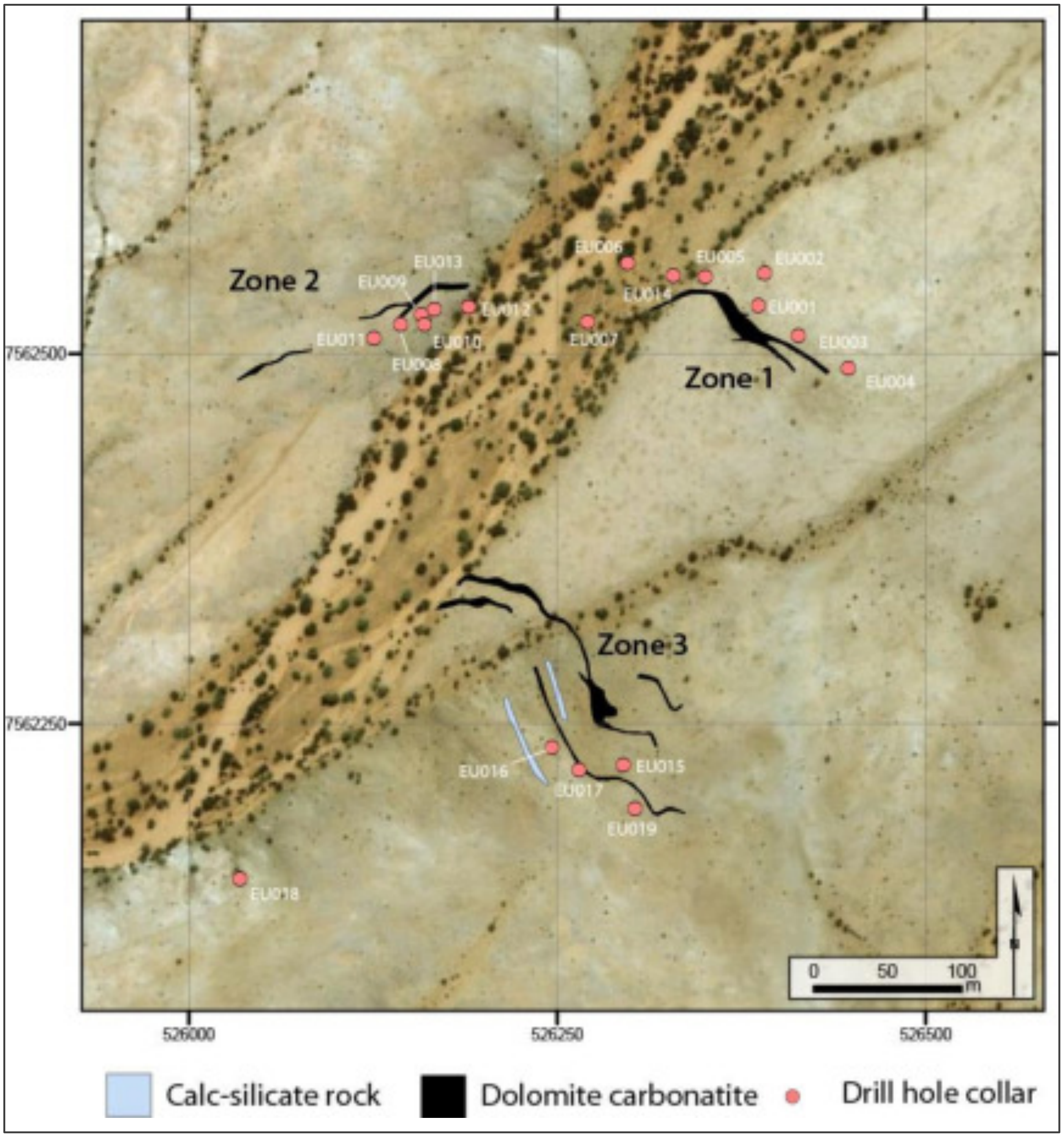

Figure 10-2: Plan map of drillhole locations relative to outcropping mineralisation

Figure 10-3: RC chip pad showing the dust and chips for each metre drilled. The red arrow demarcates carbonatite samples

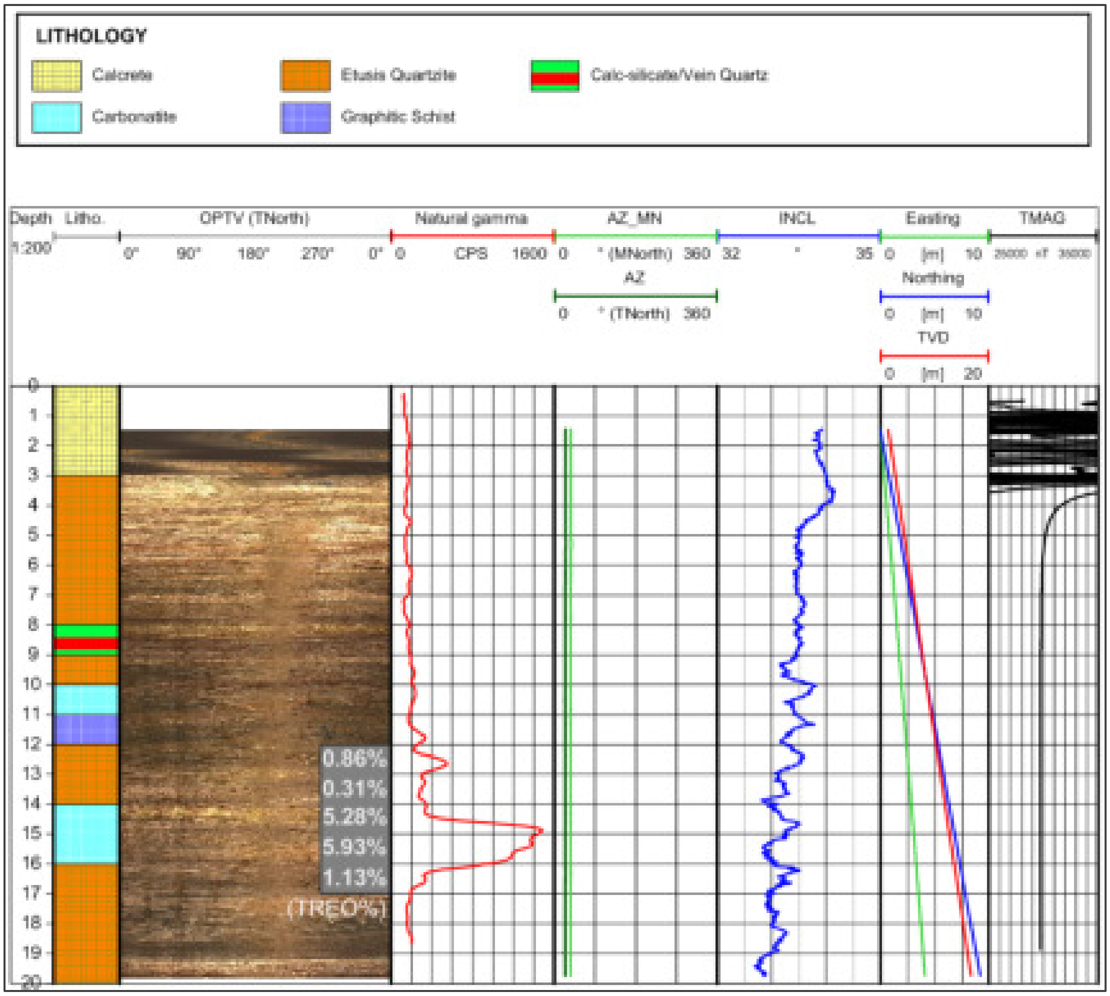

Figure 10-4: Downhole optical scan and gamma log through the mineralised carbonatite in hole EU008

10.4 Summary of Drilling Results

In total, 18 out of the 19 drillholes intersected mineralised carbonatite with an intersected length of between 1 and 9 m. It should be noted that intersected length is greater than the true width of the mineralisation when the drilling intersection is at a shallow angle.

The deepest intersection was 60 m below surface. While mineralisation was not intersected in hole EU018, which targeted an isolated radiometric anomaly below surface cover, this hole did intersect pegmatite and subsequent trenching confirmed the presence of mineralised carbonatite over half a metre with unknown orientation in the vicinity of the hole.

A table of significant drillhole intersects is provided in Table 10-1.

Table 10-1: Significant Drillhole Intersections

Hole ID	From (m)	To (m)	Intersection Length (m)	TREO %
EU001	10	16	6	5.25
and	19	24	5	1.93
EU002	8	10	2	9.36
and	55	58	3	4.8
and	61	64	3	2.23
EU003	12	13	1	8.84
and	22	23	1	9.68
EU004	11	13	2	2.49
EU005	17	26	9	8.47
EU006	32	33	1	0.34
EU007	35	36	1	0.5
EU008	14	17	3	4.11
EU009	5	7	2	0.37
EU010	12	14	2	4.97
and	16	18	2	2.48
EU011	6	7	1	3.36
and	9	10	1	0.82
EU012	31	35	4	6.47
EU013	5	8	3	0.37
EU014	12	13	1	1.82
and	29	31	2	1.74
EU015	18	24	6	1.98
EU016	14	15	1	0.22
EU017	12	15	3	1.55
EU019	20	24	4	2.92

10.5 Sample Recovery

RC sample recoveries have been estimated by recording bag weights; a plot showing average bag weight against depth is provided in Figure 10-5.

In general, the downhole bag weight reduces with depth indicating a sample recovery of 70-80%. Future exploration will assess the appropriateness of RC drilling through the application of diamond twin drillholes.

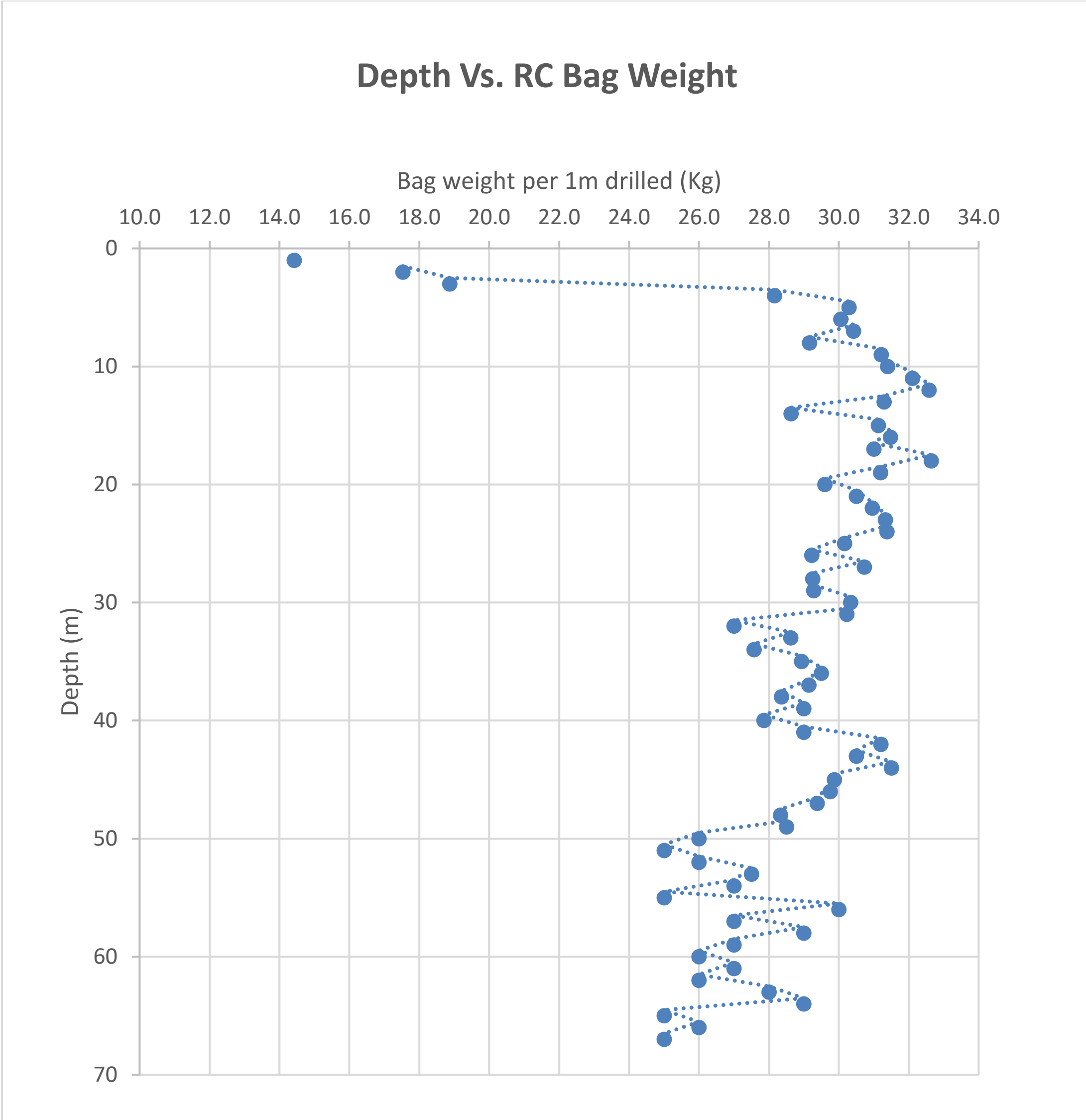

Figure 10-5: Average RC bag weights against depth downhole.

10.6 2020 & 2021 RC and Diamond Drilling

A 3.3 km RC drilling programme was completed between December 2020 and August 2021. This represented 2.3 km less than originally planned as some of the deeper RC drillholes produced undesirable wet RC samples which meant it was not possible to properly drill and sample to the desired depths. Due to this operational constraint, diamond drilling recently commenced to provide the deeper planned drilling intersections.

7 RC drillholes were completed in Zone 1 scissoring some earlier drillholes and stepping back to provide deeper intersections. 3 of the Zone 1 drillholes were stopped before reaching target depth upon encountering wet samples.

16 RC drillholes were completed in Zone 3 significantly improving the coverage achieved in the earlier drilling used for the MRE.

Five diamond drillholes were drilled starting in mid-June 2021, each 250m long. These have been collared with HQ and continued to depth with NQ diameter core. Core recovery has been good, exceeding 90%. The drillcore has been visually logged and then stored in core boxes on site ready for core sawing and sampling to be undertaken when funds are available to do so.

Three of the diamond drillholes were collared to the northeast of the RC drillholes, to step back and provide deeper intersections at a depth known to return wet RC samples. One of the diamond drillholes provides a deep scissor pair and the fifth aims to provide a long intersection through the geology under the river bed between Zone 1 and 2.

Figure 10-6 shows the collar positions of the new RC drillholes (blue) and diamond drillholes (red) in relation to trenches and the collars of the RC drillholes used for the MRE (black).

Rad Eye results, whilst not conclusive, suggest that a number of monazite-bearing dykes potentially have been intersected by the new RC drillholes. These intersects will only be confirmed to once assay results are obtained.

The samples collected from the 2020-2021 RC and diamond drilling programmes will not be submitted for assay until the RTO transaction with Battery Road is complete and the resulting issuer provides the required funds.

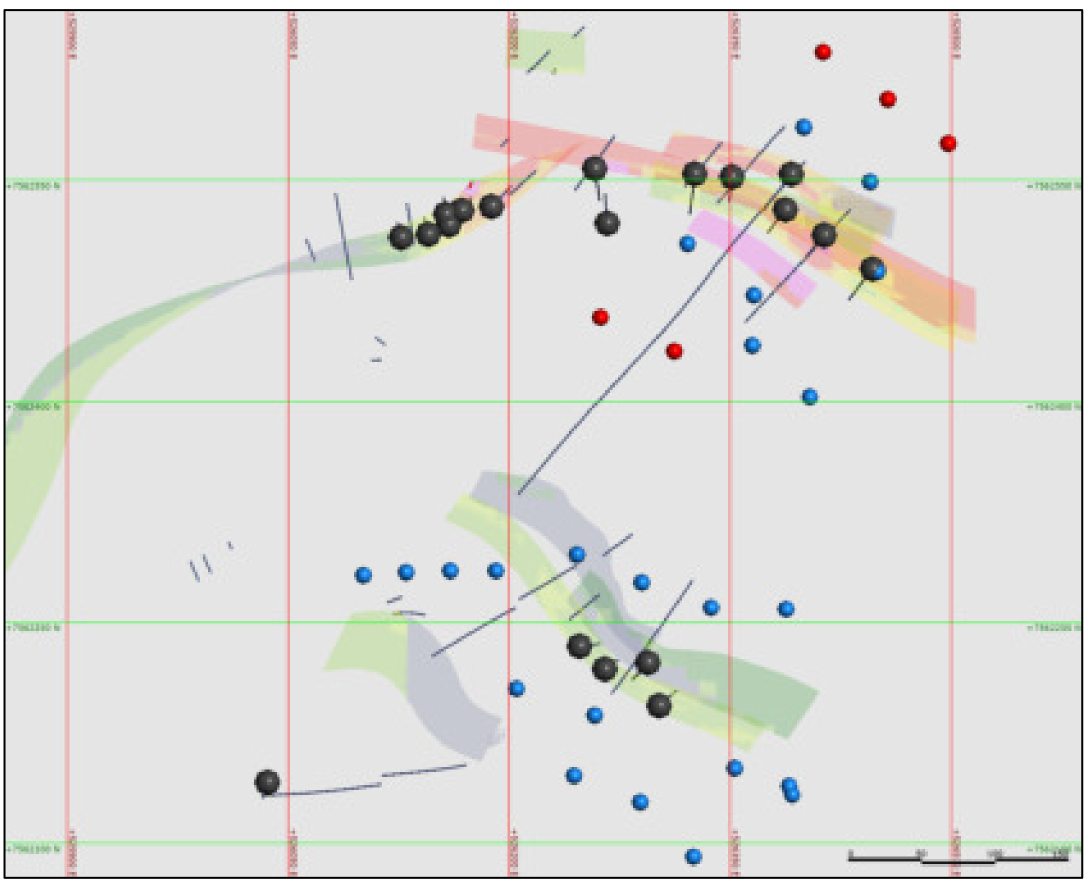

Figure 10-6: 2020-2021 RC and DD drilling locations with respect to MRE RC and trenching locations

10.7 SRK Comments

The exploration strategy used by E-Tech Namibia has been cost effective, using a traditional approach of mapping and geophysics to generate targets for more detailed investigation. The geological map interpretations rely on extrapolation which may not always be accurate. Despite this, the trenching and drilling discovery rate has been very good as a result of the geological interpretation, based on outcrops, and targeting radiometric anomalies generated by the REE-hosting monazite. Many of the most obvious targets have been sampled but there remain a number of additional targets to follow up with more trenching.

The RC drillholes and trenches for which assays are available haves delineated a number of dykes which, in some places are well defined in 3D based on mapping and trench sampling at surface extending to depth based on shallow drillhole intersections and occasional deeper drilling intersections. Trench/drill spacing is better than 20 m in parts of Zones 2 and 3 and is better than 40 m in most of Zone 1 where the best grades are encountered.

The geometry and assay distribution is sufficiently well understood to allow an Inferred Mineral Resource to be estimated.

SRK recommends additional infill trenching and drilling should be completed to improve the interpretation of the dyke continuity and thickness so that high and low grade domains can be delineated with better confidence. A significant amount of this work is part-completed, samples have been collected from 23 RC drillholes, five diamond drillholes and a number of trenches positioned to achieve these infill and expansion objectives; however, the assaying of these samples has not yet taken place and will not take place until completion of the Qualifying Transaction.

11 SAMPLE PREPARATION, ANALYSIS AND SECURITY

11.1 Introduction

This section of the report details the sample collection and analysis process as well as the QA/QC work undertaken to ensure the accuracy and precision of sample grades.

11.2 RC Drilling Sampling Procedure

Each drilled metre was collected from the rig-mounted cyclone and then split in a 7:1 (8 way) splitter, the split fraction was then split again 1:1 (2 way) to create two approximately 2 kg sub-samples. One sample was retained as a reference sample for future work, the other sample was collected as a laboratory sample stream. All sample bags were marked with the hole ID and the interval depth.

Samples to be sent for assay were selected based on lithological logging (carbonatite) and/or elevated radiation (>60 cps typically). The selected samples were re-bagged into bags marked with a sample code and a corresponding sample ticket was placed into the bag with the sample. A sample sheet was created to catalogue the samples that had been selected for analysis which was entered into the company's database. The samples were laid out for submission, photographed and then sealed into rice sacks and submitted as a single batch. An example sample batch is shown in Figure 11-1.

5% standards were inserted into the sampling stream (1 in every 20 samples). Two CRM standards are alternated and were inserted at the container shed on site prior to dispatch. 5% blanks were inserted in the sampling stream (1 in every 20 samples). The blanks were inserted at the container shed on site prior to dispatch. Duplicates were submitted at 5% into the sample stream (1 in every 20 samples) and was generated through splitting of the 25% process sample at the container shed. Each sample was provided with a unique sample number and the duplicate and originals were inserted seamlessly into the sample stream.

The reference sample and the remaining samples from the laboratory sample stream were then stored in a secure container for future analysis, if required.

Figure 11-1: Samples ready for dispatch

11.3 Trench Sampling Procedure

Sampling of the trenches was conducted for each metre along the length of the trench by creating 1 m composite chip samples for each interval. Starting in 2017, sampling was limited to intervals which returned anomalous Rad-Eye CPS results.

For each sampled metre, approximately 3–4 kg of material was collected for analysis by channel sampling with a geologist's pick through the largely friable material exposed in the trenches. Each sample was assigned a unique sample code from a sample ticket book and a corresponding ticket stub was inserted into each bag. CRM, blank and duplicate samples were then inserted into the sample series following the same methodology as described for the RC drilling.

11.4 Sample Preparation

Samples were transported to Windhoek by Dr Tim Smalley in a 4x4 vehicle covered by tarpaulin. Sample preparation was undertaken at Activation Laboratories Ltd. ("Actlabs") Namibia PTY using the RX1 methodology for both RC samples and trench samples. This sample preparation involves crushing the sample to 90% passing 2 mm, riffle splitting a 250 g sub-sample and pulverizing to 95% passing 105 µm. E-Tech Namibia staff conducted an inspection of the sample preparation laboratory prior to submission and found it to be clean and well organised.

11.5 Sample Analysis

After sample preparation, a 50 g pulp was submitted to Actlabs Ancaster- Ontario, Canada for REE analysis by method 8-REE. The analytical method, utilized for both RC samples and trench samples, is described below:

- Sample ground to 95%-200 mesh to ensure complete fusion of resistate minerals;
- Lithium metaborate/tetraborate fusion;
- Analysis by ICP-OES and ICP-MS; and
- Mass balance calculated as an additional quality control technique to ensure complete analysis.

Analytical detection limits for the elements and oxides analysed by Actlab Ancaster's 8-REE method are presented in Table 11-1.

Table 11-1: Analytical detection limits: Actlabs 8-REE method

Element	Detection Limit (%)	Element	Detection Limit (ppm)	Element	Detection Limit (ppm)	Element	Detection Limit (ppm)
Al_2O_3	0.01	Ag	0.5	Ge	1	Sm	0.1
CaO	0.01	As	5	Hf	0.2	Sn	1
Fe_2O_3	0.01	Ba	3	Ho	0.1	Sr	2
K_2O	0.01	Be	1	In	0.2	Ta	0.1
LOI	0.01	Bi	0.4	La	0.1	Tb	0.1
MgO	0.01	Ce	0.1	Lu	0.04	Th	0.1
MnO	0.001	Co	1	Mo	2	Tl	0.1
Na_2O	0.01	Cr	20	Nb	1	Tm	0.05
P_2O_5	0.01	Cs	0.5	Nd	0.1	U	0.1
SiO_2	0.01	Cu	10	Ni	20	V	5
TiO_2	0.001	Dy	0.1	Pb	5	W	1
		Er	0.1	Pr	0.05	Y	2
		Eu	0.05	Rb	2	Yb	0.1
		Ga	1	Sb	0.5	Zn	30
		Gd	0.1	Sc	1	Zr	4

11.6 Laboratory Accreditation

Actlabs Ancaster is ISO 17025 accredited and/or certified to 9001: 2008

11.7 QA/QC Samples

Standards, blanks and field duplicates were added into the sample sequence every 15 to 20 samples, as noted in Section 11.2 and 11.3.

Two REE standards were used both of which are Certified Reference Materials (“CRM”), sourced from Geostats PTY. GRE-02 (4.31% TREO) and GRE-06 (41.71% TREO). A total of 12 CRM were inserted into the sample stream, 4 low grade GRE02 CRM and 8 high grade GRE06 CRM.

Blank material was sourced locally from weathered marble material, taken from the Karibib Marble formation and is considered to be free from REE.

Field duplicates were created by splitting the original sample into two sub samples, each of which was assigned a unique sample code and inserted into the sample stream. A total of 346 normal samples and 30 QA/QC samples have been submitted for analysis. The overall insertion rate for each QA/QC sample type is presented in Table 11-2 below.

Table 11-2: Insertion rates for QA/QC samples

Sample Type	Number Inserted	Percentage of samples
Field Duplicate	10	3
Standard GRE-02	4	1
Standard GRE-06	8	2
Blank	8	2
Total	**30**	**8**

11.8 QA/QC Analysis

11.8.1 Standards

All 12 CRM returned assay values within two standard deviations of the stated CRM grade for the 4 main elements of interest (Cerium, Praseodymium, Lanthanum and Neodymium). A graphical analysis of CRM GRE02 is provided for each of the main elements of interest in Figure 11-2 to Figure 11-5. A graphical analysis of CRM GRE06 is provided for each of the main elements of interest in Figure 11-6 to Figure 11-9.

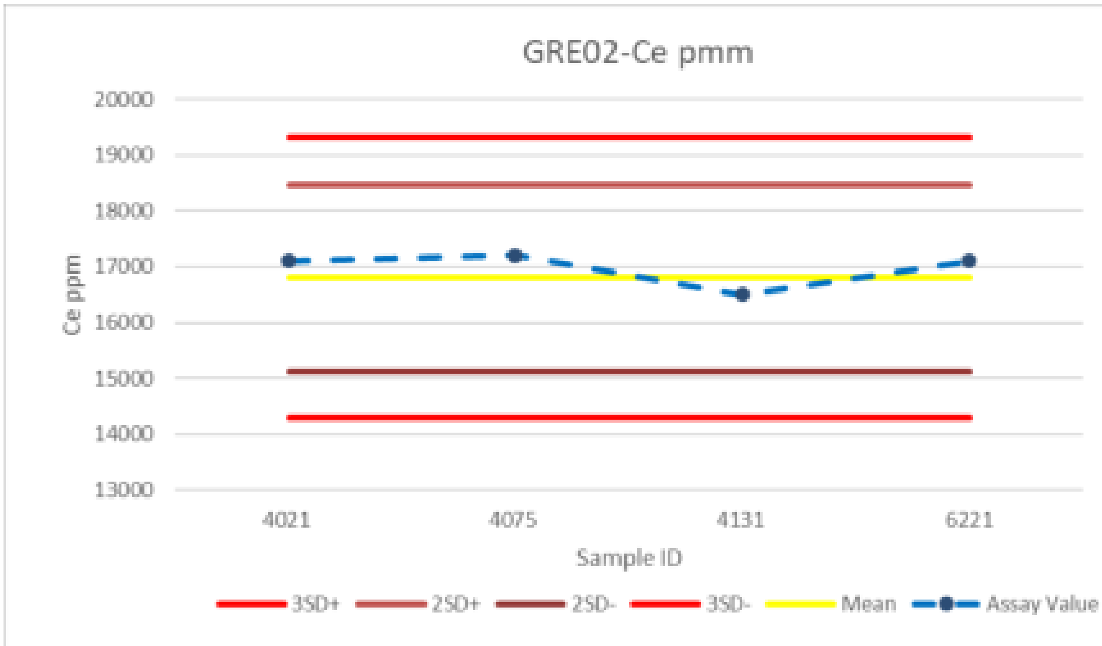

Figure 11-2: GRE02 CRM performance for Ce

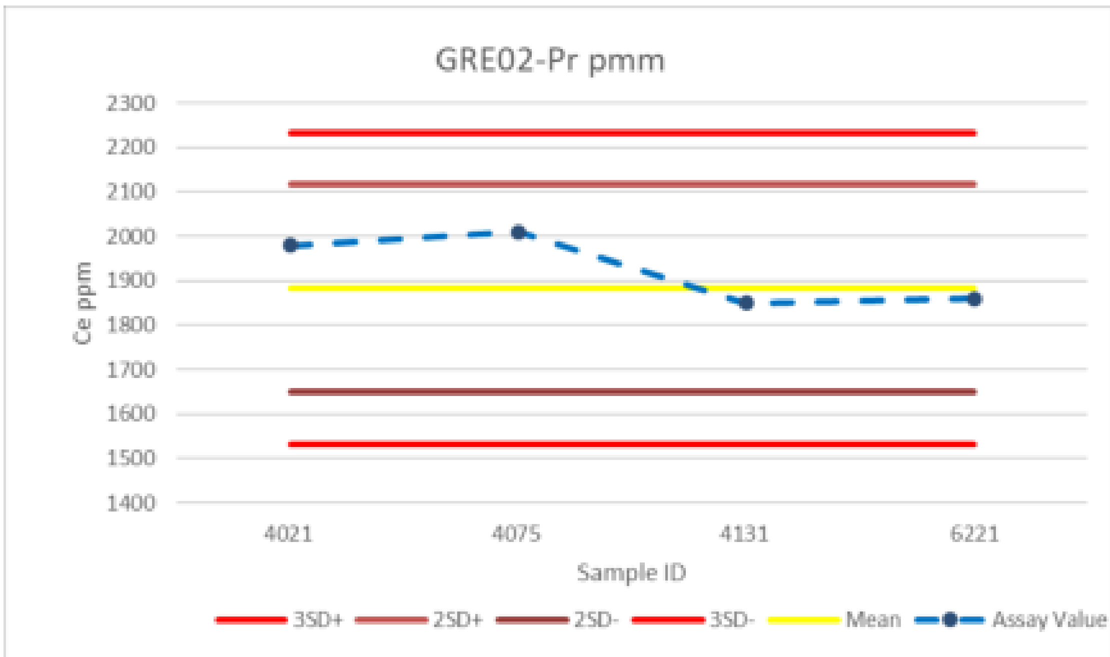

Figure 11-3: GRE02 CRM performance for Pr

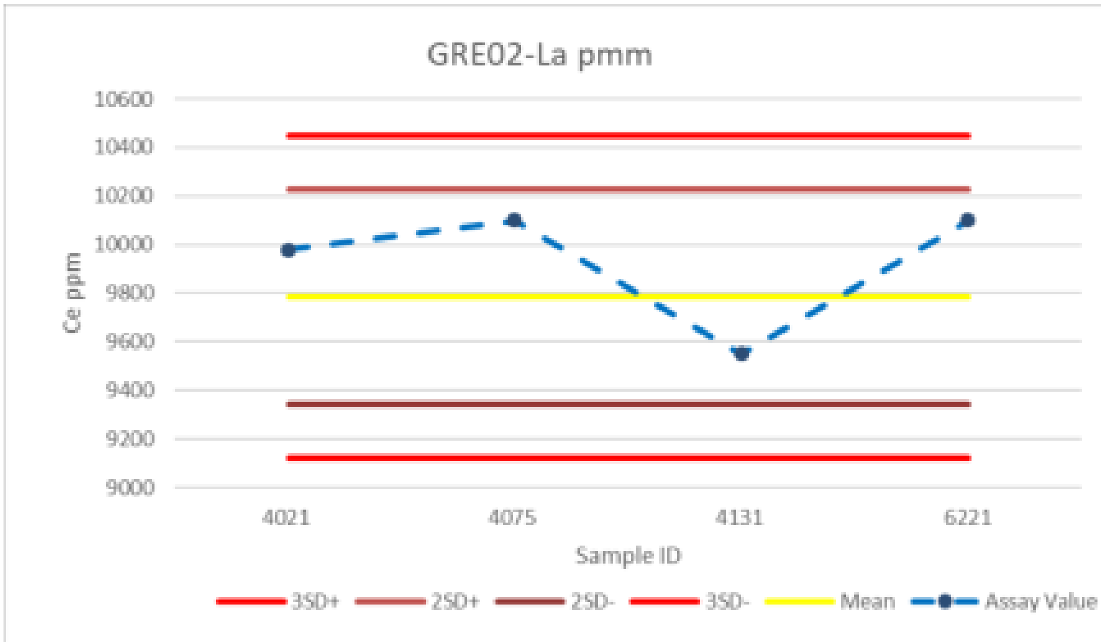

Figure 11-4: GRE02 CRM performance for La

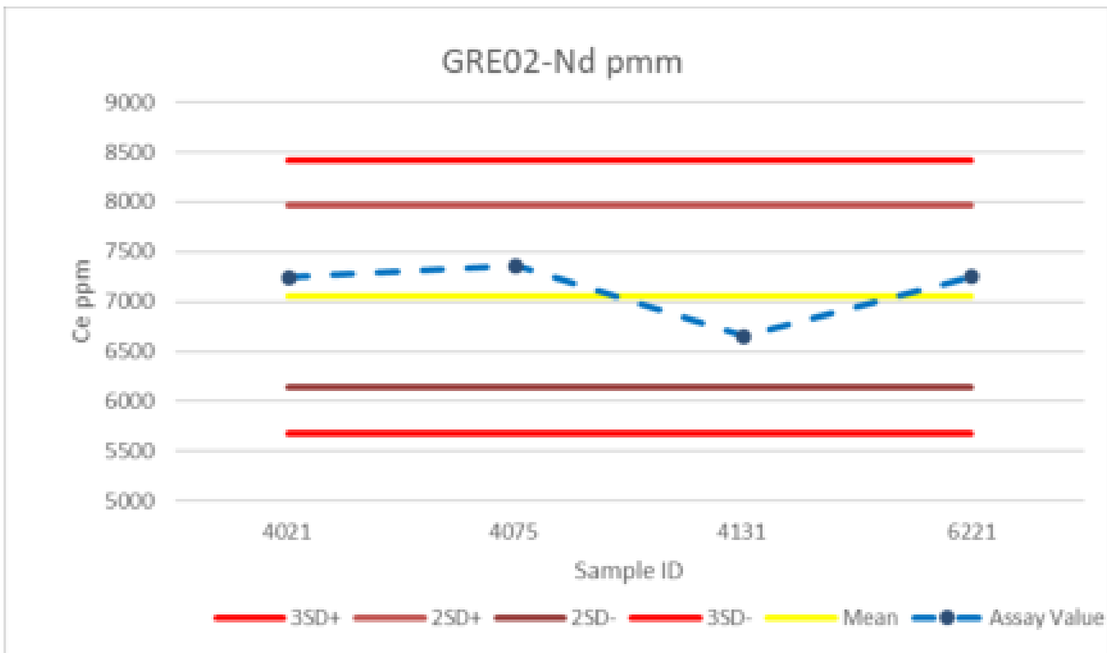

Figure 11-5: GRE02 CRM performance for Nd

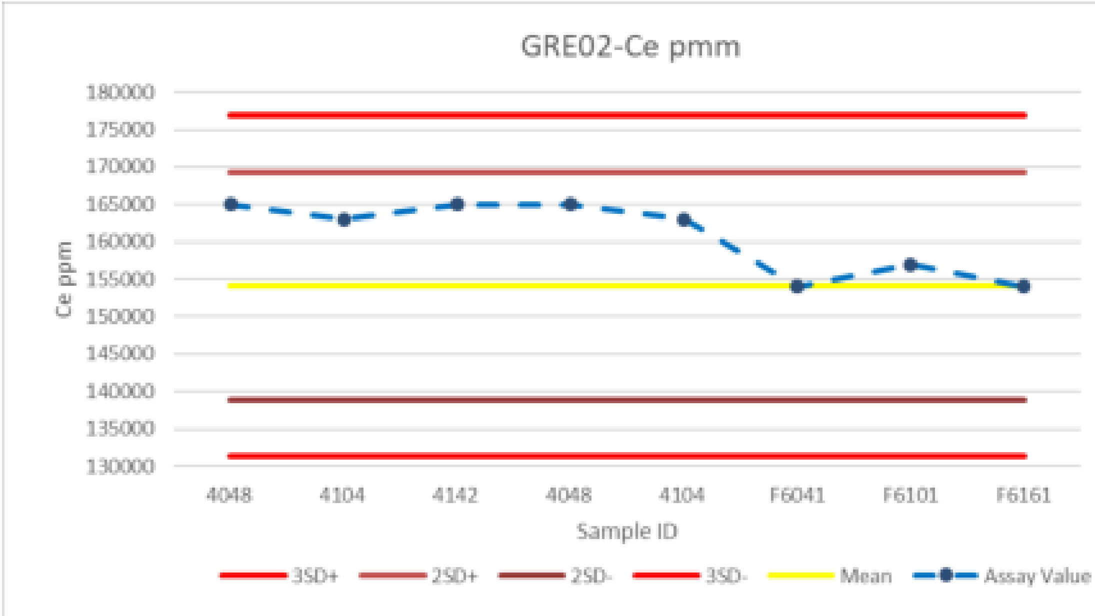

Figure 11-6: GRE06 CRM performance for Ce

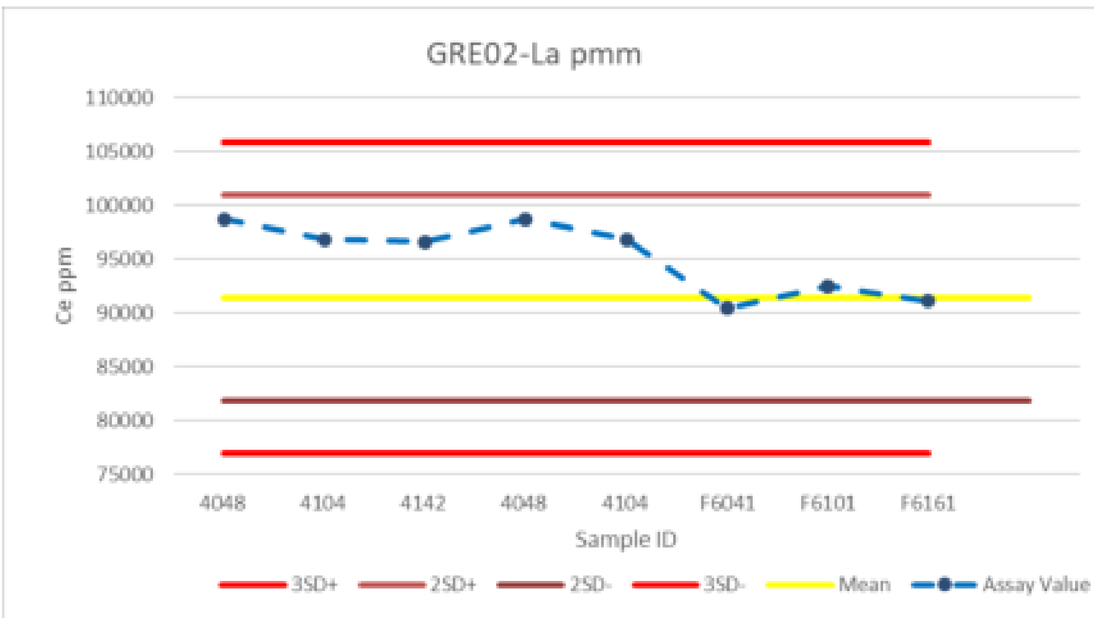

Figure 11-7: GRE06 CRM performance for La

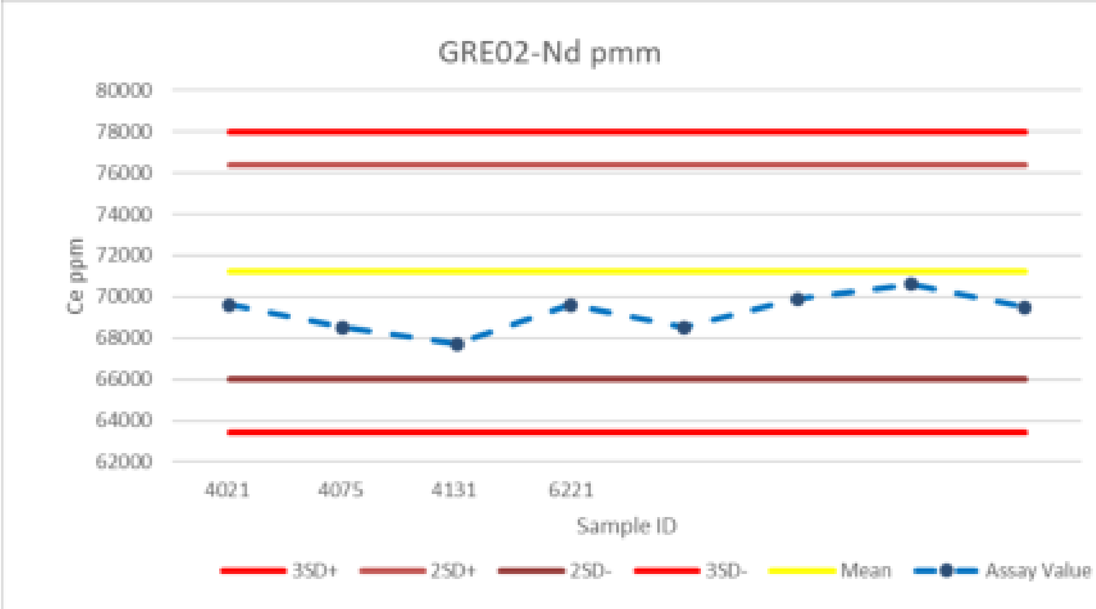

Figure 11-8: GRE06 CRM performance for Nd

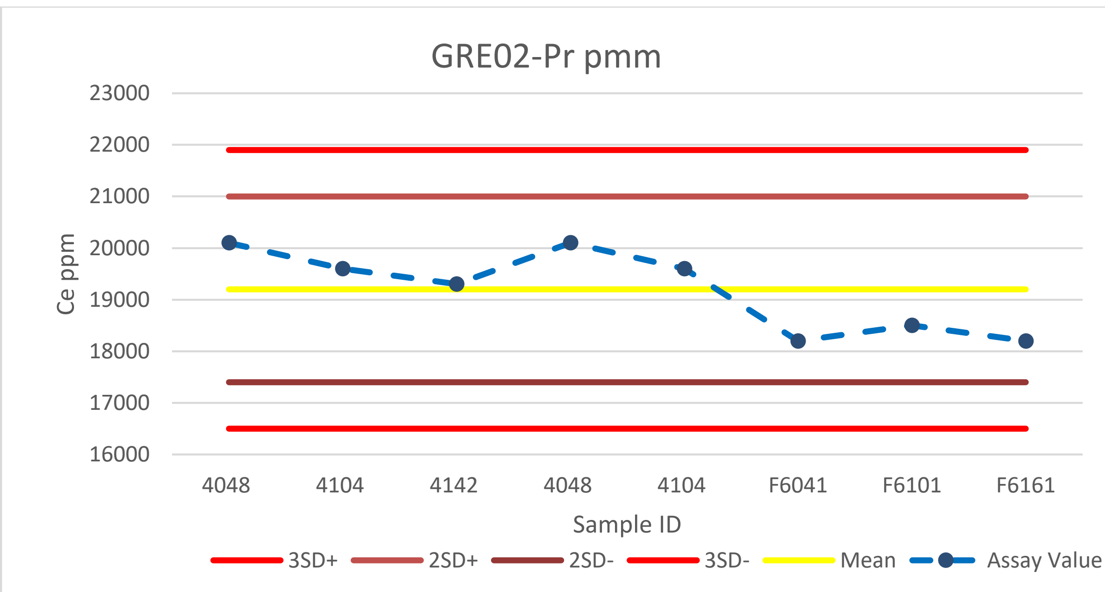

Figure 11-9: GRE06 CRM performance for Pr

11.8.2 Blanks

A total of 8 blank samples were inserted into the sample stream. The performance of the blank samples is considered acceptable and does not indicate any contamination between samples. A graphical analysis of blank performance is presented in Figure 11-10.

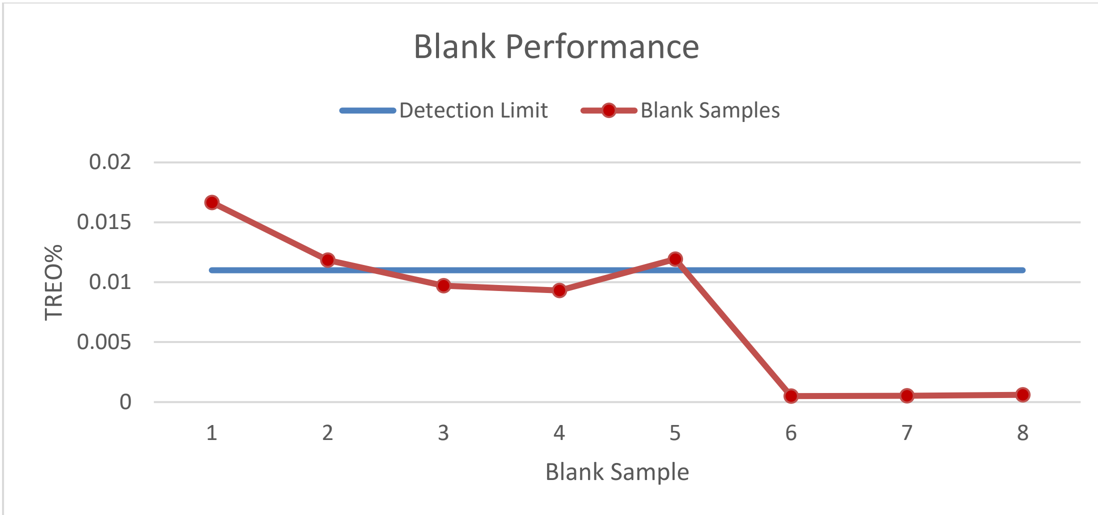

Figure 11-10: Blank performance

11.8.3 Duplicates

Analytical precision and sample variability has been monitored by submitting field duplicates for analysis as part of the sample stream. The performance of the duplicate samples indicates good analytical precision and limited grade-variability within the homogenised samples. A graphical analysis of duplicate performance is provided in Figure 11-11.

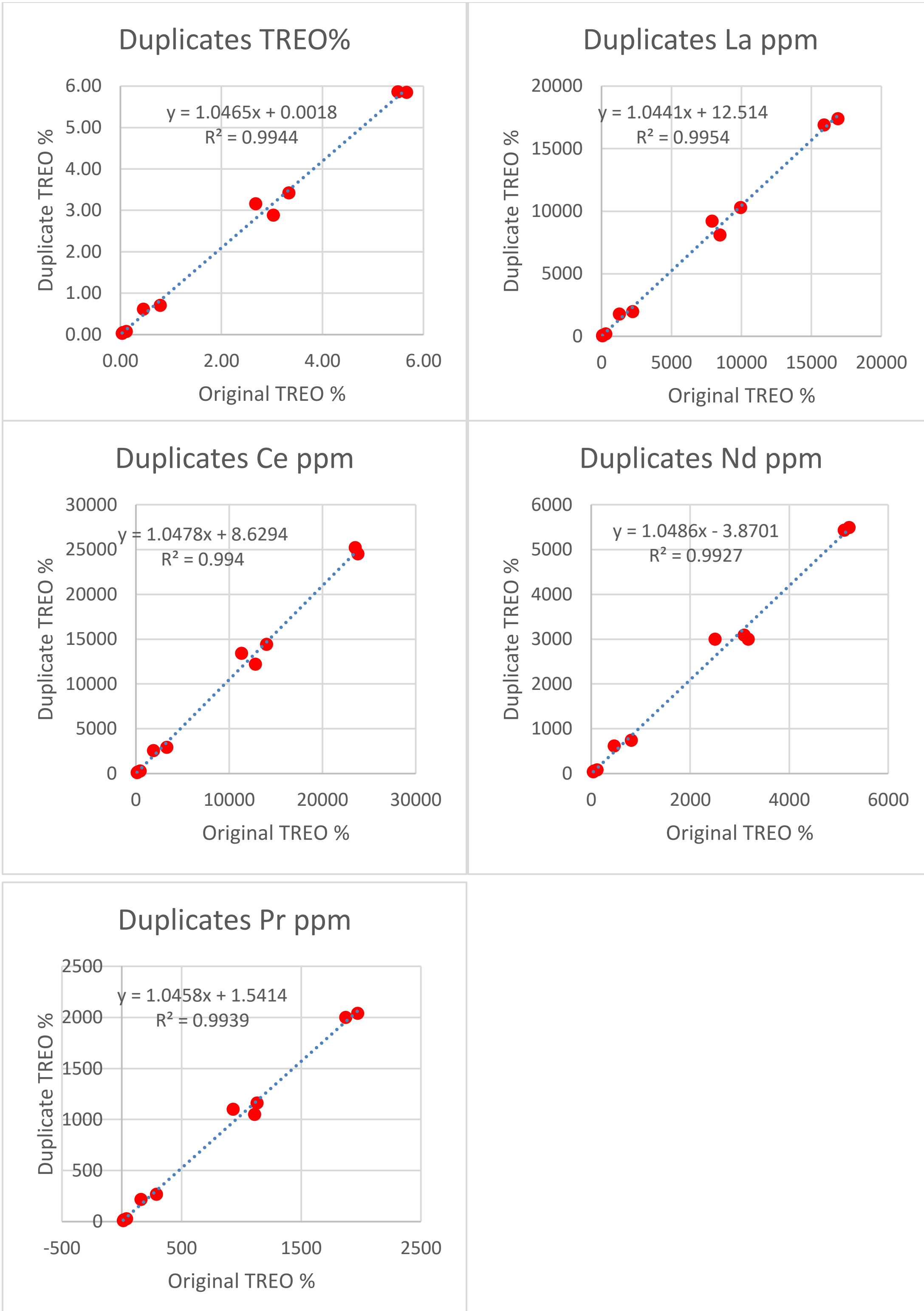

Figure 11-11: Field duplicate performance

11.9 TREO Determination

Total Rare Earth Oxides (TREO) is the industry-standard form of reporting REE grades. It is the sum of the oxides of trivalent rare earths (REE_2O_3). TREO contents are calculated by multiplying the elemental concentration reported by the laboratory by the conversion factors provided in Table 11-3. To convert from ppm to %, the values are divided by 10,000.

When considering the light, medium and heavy rare earth elements (LREE, MREE and HREE), the approach differs between companies. E-Tech Namibia uses the scheme provided in Table 11-3. Note, as is often the case, yttrium is included in the HREE group, it behaves like a rare earth but is not officially categorised as a rare earth element.

Table 11-3: REE Groupings and conversion factors for REO

REE type	Element name	Symbol	Oxide	Conversion factor
HREE	Yttrium	Y	Y_2O_3	1.2699
LREE	Lanthanum	La	La_2O_3	1.1728
	Cerium	Ce	Ce_2O_3	1.1713
	Praseodymium	Pr	Pr_2O_3	1.1703
	Neodymium	Nd	Nd_2O_3	1.1664
MREE	Samarium	Sm	Sm_2O_3	1.1596
	Europium	Eu	Eu_2O_3	1.1579
	Gadolinium	Gd	Gd_2O_3	1.1526
HREE	Terbium	Tb	Tb_2O_3	1.1510
	Dysprosium	Dy	Dy_2O_3	1.1477
	Holmium	Ho	Ho_2O_3	1.1455
	Erbium	Er	Er_2O_3	1.1435
	Thulium	Tm	Tm_2O_3	1.1421
	Ytterbium	Yb	Yb_2O_3	1.1387
	Lutetium	Lu	Lu_2O_3	1.1371

11.10 SRK Comments

The sample collection methods used for RC drilling and trenching and the subsequent sample preparation methods are standard for exploration projects. The QAQC programme with an 8% sample submission rate is appropriate at this early stage whilst total sample numbers are relatively low. The higher grade TREO CRM is of only limited usefulness in SRK's opinion, as it is much higher grade than the deposit and will be more useful to quality control the grade determinations of mineral concentrate in due course. SRK has therefore recommended that the Company identifies alternative commercially available materials and ensures these are matrix matched as far as possible, or alternatively invests in creating project specific standards using RC reject samples.

The field duplicates show that the mineralisation is reasonably homogeneous within each drill sample and that very little error is introduced in the sample splitting process; the duplicate and CRM results together demonstrate consistent performance by the assay laboratory.

12 DATA VERIFICATION

SRK has not witnessed samples being taken in the field, however, Mr Keith Webb, was able to observe and verify trench and drillhole locations, make geological observations and visit the sample storage facility and sample preparation laboratory.

E-Tech Namibia's well documented working practices coupled with the QAQC programme generally support the accuracy of the laboratory, provide sufficient confidence in the quality of the data supporting the Mineral Resource estimate presented in Section 14. Independent sampling, however, metallurgical testwork samples have provided external corroboration of the grades encountered at the project.

SRK has undertaken a spot check of database entries against assay laboratory certificates and found there to be no errors in those entries that were checked.

Overall, despite the risks generally associated with relying on data generated by a project operator, the QP has sufficient confidence in the Mineral Resource estimates presented in this Technical Report and the data upon which these are based.

13 MINERAL PROCESSING AND METALLURGICAL TESTING

13.1 Introduction

In Q4 2016, E-Tech Namibia collected a 300 kg bulk sample of mineralised dolomite carbonatite from a test pit in Zone 1; this was used for metallurgical testing at SGS Mineral Services UK ("SGS"). The sample was taken from historical pitting in Zone 1 shown in Figure 13-1. The sample is shown prior to submission in Figure 13-2. The sample was subsequently split down to a 100 kg sub-sample and submitted to SGS for gravity release analysis across a range of size fractions. The remaining 200 kg is in container storage in the UK. Head grades of the sample received by SGS, as determined by the Wheal Jane assay laboratory, are presented in Table 13-1.

During Q4 2019 E-Tech Namibia collected a 1 t bulk sample of fresh carbonatite from a test pit for further metallurgical testing by Bond Equipment of Klerksdorp, South Africa where the material is currently stored. When funds allow, this testwork will further develop and optimise the processing flowsheet design for a potential gravity plant.

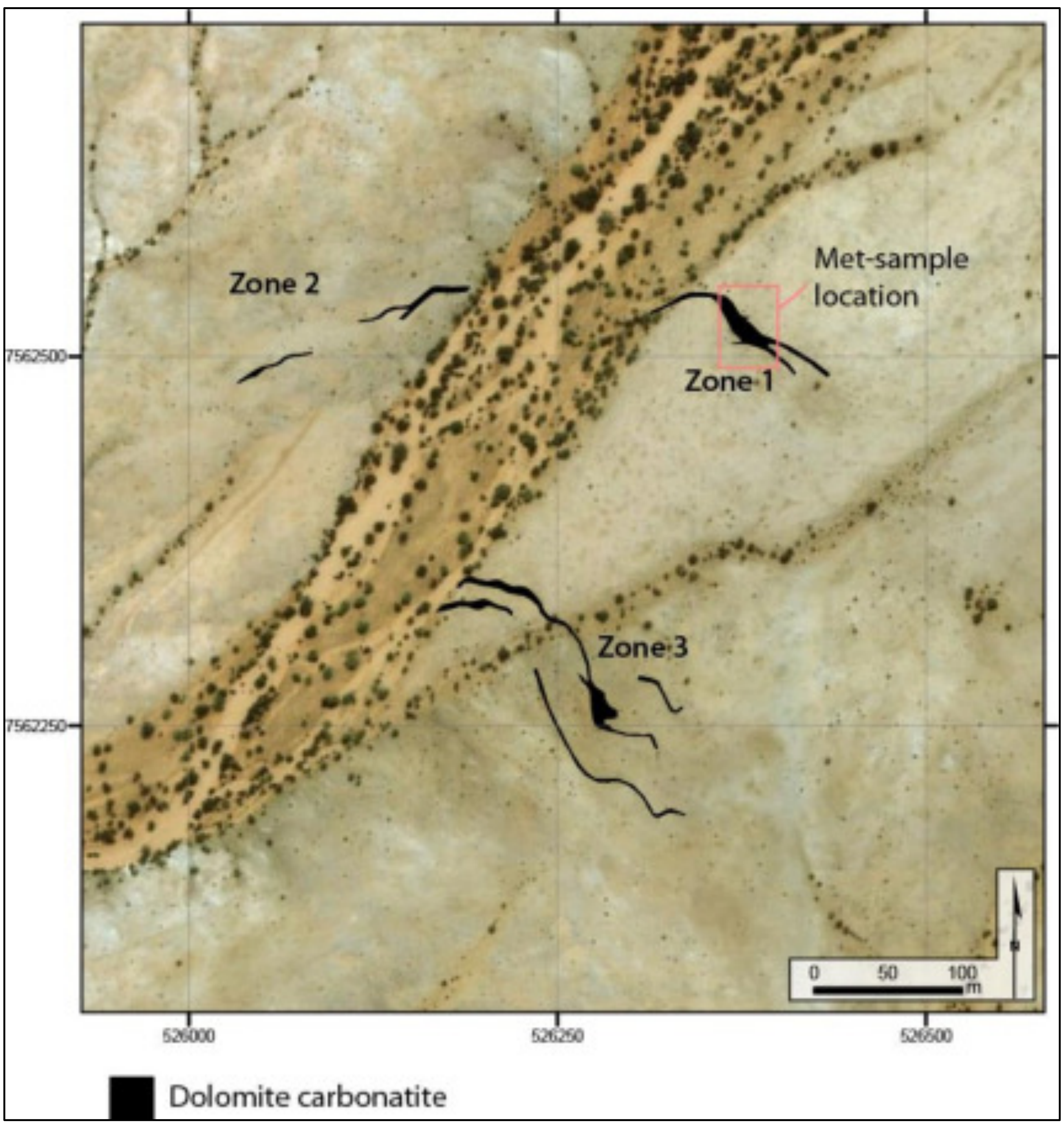

Figure 13-1: Plan showing the location of the surface metallurgical sample

Table 13-1: SGS metallurgical sample head grades

Element	Grade (%)
Fe	6.08
P_2O_5	2.24
Ce	3.05
La	2.17
Nd	0.681
Pr	0.24

Head grade analysis was undertaken by Wheal Jane Laboratory (UK) via Inductive Coupled Plasma Optical Emission Spectrometry (“ICP-OES”). Wheal Jane Laboratory is a United Kingdom Accreditation Service (“UKAS”) accredited testing laboratory. Environmental and management control systems meet as a minimum ISO 9001, ISO 14001 and ISO 17025 requirements.

Figure 13-2: 300 kg bulk metallurgical sample before shipping to UK

13.2 Size Fraction Analysis

Liberation of the REE-bearing monazite occurred at all size fractions tested, with the best liberation characteristics attained below 250 μm and best concentration of monazite achieved in the -125 to +75 μm size range. A sieved size fraction analysis graph for P_2O_5 (a proxy for monazite and therefore REE) is presented in Figure 13-3.

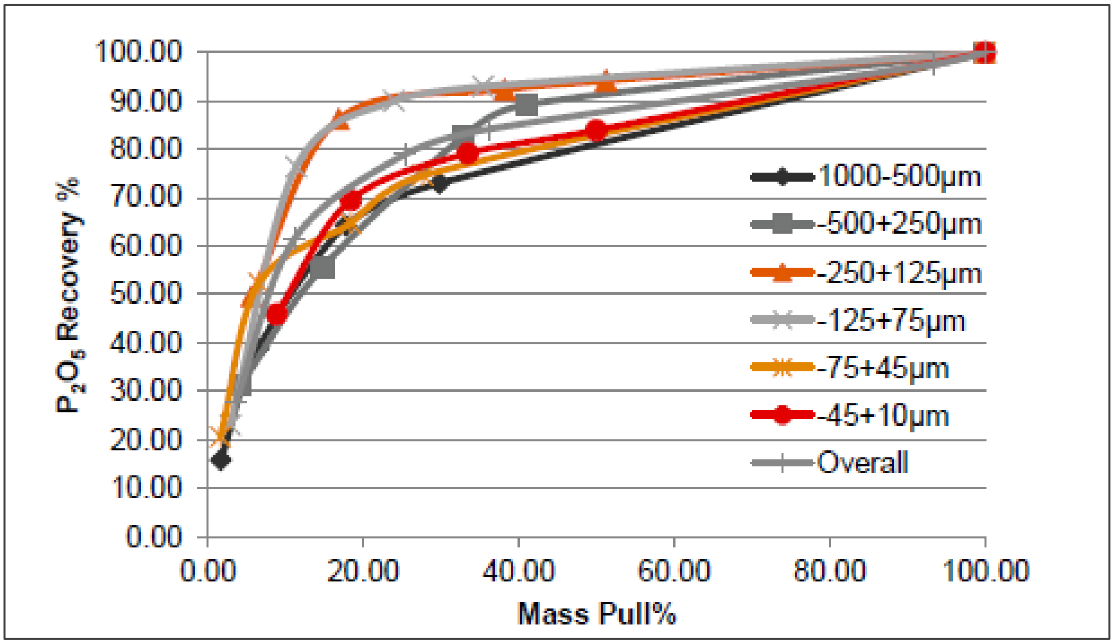

Figure 13-3: Recovery vs mass pull % for a range of grind sizes

13.3 Gravity Separation

A sub-sample of 90 kg was milled to a P_{80} of 250 µm. The sample was processed on a Holman 2000 shaking table. An unsorted first-pass recovery of P_2O_5 of 65% to gravity concentrate was achieved on the unwashed grind for a mass pull of approximately 10%. The sample under processing is shown in Figure 13-4. The initial gravity recovery may be improved with further investigation of the middlings and tailings fractions, with further particle size analysis and mineralogy.

Figure 13-4: Shaking table test separation of monazite (red zone) and magnetite (black zone)

The resulting gravity concentrate graded 25.41 % Fe, approximately 50% of which is contained within magnetite, 15.44% P_2O_5, 13.9% La, 4.26% Nd and 1.59% Pr.

13.4 Magnetic Separation

Dry low-intensity magnetic separation of the gravity concentrate removed magnetite and further improved the concentrate grades to 19.73% P_2O_5, 17.77% La, 5.45% Nd, and 2.12% Pr. The magnetite recovery to the low intensity magnet was 99% efficient without loss of REE. The gravity concentrate under magnetic separation is shown in Figure 13-5.

Figure 13-5: Magnetite removal from Eureka monazite concentrate

Figure 13-6: Eureka monazite concentrate

The final post gravity and magnetic separation concentrate is shown in Figure 13-6.

Recommendations from SGS for impoved recovery include investigating rougher-scavenger-cleaner optimisation of the fine gravity circuit with potential regrind on the midlings fraction.

The results of the SGS metallurgical testing are shown in Table 13-2.

Table 13-2: Summary results for gravity and magnetic processing testwork

Gravity 250µm 1st-pass unwashed							
Element	**Assayed Head grade**	**Gravity concentrate grade**	**Recovery**	**Middlings grade**	**Recovery**	**Tailings grade**	**Recovery**
Fe mag							
Fe	**6.08%**	**25.41%**	33.38%	**7.78%**	14.09%	**5.17%**	52.53%
P_2O_5	**2.24%**	**15.44%**	65.29%	**0.96%**	5.60%	**0.89%**	29.11%
Ce	**3.05%**	**19.80%**	65.96%	**1.24%**	5.69%	**1.10%**	28.36%
La	**2.17%**	**13.90%**	65.93%	**0.87%**	5.69%	**0.78%**	28.38%
Nd	**0.68%**	**4.26%**	65.48%	**0.27%**	5.70%	**0.24%**	28.82%
Pr	**0.24%**	**1.59%**	69.01%	**0.09%**	5.24%	**0.08%**	25.75%
SEG & HREE	**0.07%**	**0.57%**	60.00%	**0.04%**	5.50%	**0.04%**	34.50%
TREE	**6.21%**	**40.12%**		**2.51%**		**2.24%**	
TREO (converted to oxide)	**7.27%**	**46.98%**	65.28%	**2.94%**	5.56%	**2.62%**	29.16%
After First Magnetic Separation							
Element	**Assayed Head grade**	**Grade non-mag conc**	**Stage Recovery**	**Grade mag conc**	**Stage Recovery**		
Fe mag		**0.10%**	0.64%		99.4%		
Fe	**6.08%**	**5.25%**	26.40%	**61.97%**	73.6%		
P_2O_5	**2.24%**	**19.73%**	99.76%	**0.20%**	0.2%		
Ce	**3.05%**	**24.60%**	99.48%	**0.54%**	0.5%		
La	**2.17%**	**17.70%**	99.52%	**0.35%**	0.5%		
Nd	**0.68%**	**5.45%**	99.49%	**0.12%**	0.5%		
Pr	**0.24%**	**2.12%**	99.78%	**0.20%**	0.2%		
SEG & HREE	**0.07%**	**0.78%**	99.50%	**0.30%**	0.5%		
TREE	**6.21%**	**50.65%**		**1.51%**			
TREO (converted to oxide)	**7.27%**	**59.31%**	99.55%	**1.76%**	0.4%		

13.5 Monazite Chemistry

The REE at Eureka is contained within monazite. In-situ analysis of the major elements (those above ~0.25 wt.%) in monazite grains was undertaken at Camborne School of Mines by Electron Probe Micro Analysis (“EPMA”). In order to evaluate the full deportment of REE in the monazite, additional in-situ trace element analyses by Laser-Ablation ICP MS (“LA-ICPMS”) were undertaken at Leeds University. The results of the EPMA and LA-ICPMS analyses are presented in Table 13-3 and Table 13-4 below. Monazite is enriched in LREE compared to HREE, as represented in the chondrite normalised plot in Figure 13-7.

Table 13-3: EPMA analyses of monazite grains

	P_2O_5	SiO_2	La_2O_3	Ce_2O_3	Pr_2O_3	Nd_2O_3	Sm_2O_3	Gd_2O_3	Ho_2O_3	CaO	SrO	ThO_2	UO_2	F	Total
Average wt. %	31.26	0.23	24.46	32.69	2.45	8.03	0.39	0.18	0.09	0.08	0.18	0.63	0.06	0.13	100.49
St Dev (1σ)	0.30	0.20	2.21	0.49	0.33	1.01	0.10	0.02	0.01	0.03	0.07	0.13	0.01	0.03	0.83
n=	93	28	93	93	93	93	71	2	3	92	79	93	53	4	93

Table 13-4: LAICPMS analyses of monazite grains

	Sr	Y	Ba	La	Ce	Pr	Sm	Eu	Gd	Tb	Dy	Ho	Er	Tm	Yb	Lu	Pb	Th	U
Average ppm	1765	140	9	261000	347000	23200	2680	430	1250	44	76	6.4	8.1	0.50	1.4	0.2	180	5500	90
St Dev (1σ)	890	50	5.5	42000	34500	1000	300	75	86	6	17	1.6	2.2	0.2	0.6	0.1	30	900	40
n=	60	60	59	60	60	60	60	60	60	60	60	60	60	60	60	59	60	60	60

*Nd not reported as this is used to calibrate LAICPMS equipment

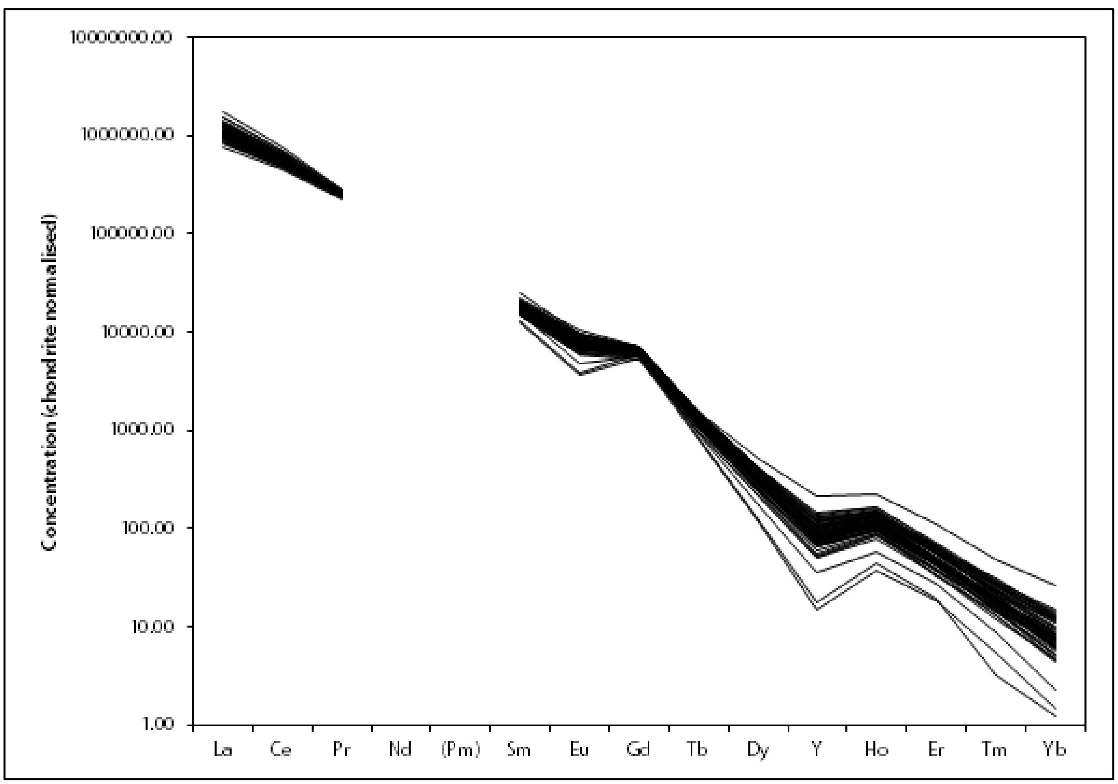

Figure 13-7: Chondrite normalised plot displaying REE distribution in monazite from Eureka

Multiple EPMA spot analyses of the monazite grains confirm a consistency to the fractionation of REE and actinides (Th & U). This shows the absence of geochemical zonation within the monazite grains and generally homogeneous chemistry of the monazite at Eureka.

With regard to thorium content, the standard deviation is narrow from both sets of analyses. The consistency of this relatively low thorium grade in the Eureka monazite is positive for future material handling purposes - the implications of this are described in more detail in Section 13.6. Thorium is strongly correlated with phosphorus and REE grades as illustrated in Figure 13-8 below, indicating that thorium occurs almost exclusively in monazite.

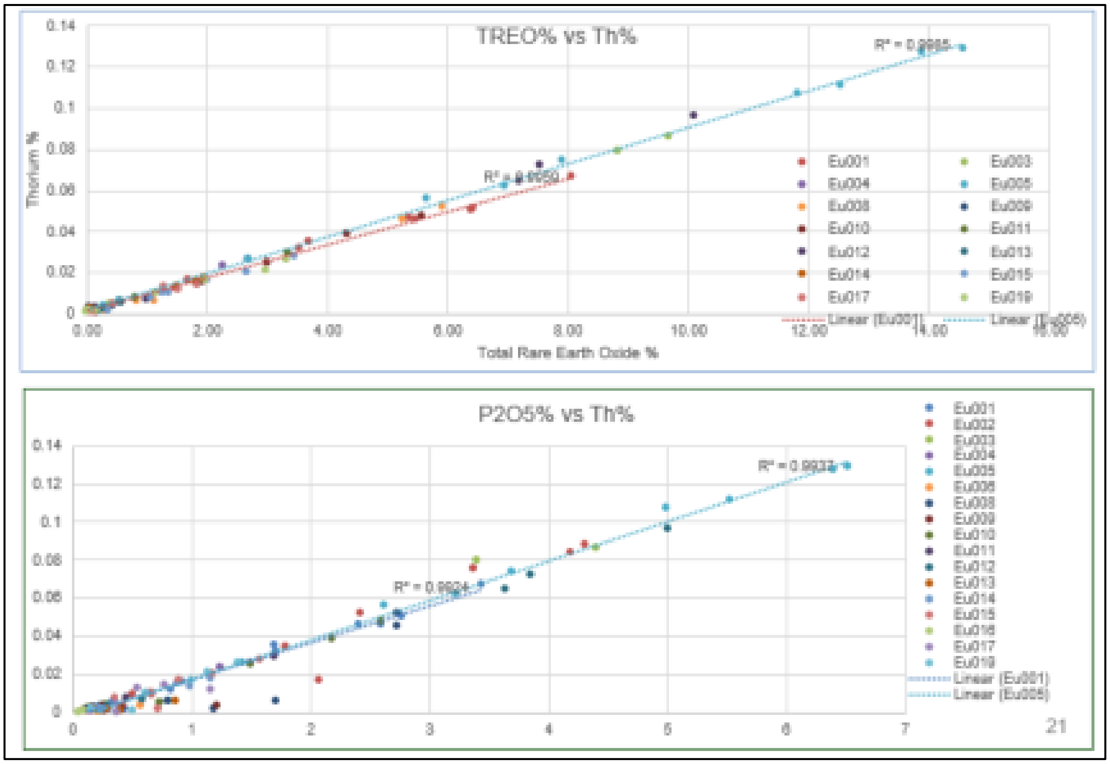

Figure 13-8: TREO vs Th and P_2O_5 grades

13.6 Assessment of Concentrate Radioactivity

13.6.1 Background

REE ore concentrates typically contain traces of thorium (Th) and uranium (U) and are considered as "naturally occurring radioactive materials" ("NORM") under international classification.

13.6.2 Referee analysis on concentrate product

The initial metallurgical testwork undertaken by SGS produced a concentrate that was analysed by Wheal Jane Laboratory Services using peroxide fusion Optical Emission Spectrometry ("ICP-OES") which does not produce accurate Th and U data. A sub-sample of the same concentrate product was therefore sent to Actlabs (Canada) in September 2017 for referee analysis using ICP-MS which is more accurate for analysing U and Th.

The Actlabs analysis of the concentrate product shows much lower Th and U than reported by Wheal Jane Laboratory resulting in a specific activity of 19.5 Bq/g compared with 50 Bq/g based on the original Wheal Jane assay.

The referee analysis of the 1st pass magnetic concentrate (showing a 88% pure monazite concentrate with 0.43 wt.% Th) corresponds well with Electron Probe Micro Analysis ("EPMA") and Laser-Ablation ICP MS ("LA-ICPMS") multi-spot analyses of the 100% monazite grains which give a Th content of 0.6% Th, supporting the Actlabs ICP-MS in favour of the Wheal Jane grades.

The results of the referee analysis are presented in Table 13-5 below. Results are also provided for a further dry magnetic separation pass conducted by E-Tech Namibia staff using a permanent bar magnet prior to submission to Actlabs. The additional dry magnetic separation undertaken by E-Tech Namibia staff shows improved TREO values over the single pass magnetic separation.

Table 13-5: Comparison of Wheal Jane assays with Actlabs referee assays

Element	Gravity concentrate grade		After First Pass Magnetic Removal		After Second Pass Magnetic Removal
	Wheal Jane	Actlabs referee	Wheal Jane	Actlabs referee	Actlabs only
Fe mag			0.10%		
Fe	25.41%	**23.90%**	5.25%	**8.08%**	**4.72**
P_2O_5	15.44%	**19.99%**	19.73%	**24.50%**	**26.4**
Ce	19.80%	**20.60%**	24.60%	**25.10%**	**25.4**
La	13.90%	**13.70%**	17.70%	**16.30%**	**16.6**
Nd	4.26%	**4.55%**	5.45%	**5.57%**	**5.94**
Pr	1.59%	**1.70%**	2.12%	**2.04%**	**2.14**
SEG & HREE	0.57%	**0.38%**	0.78%	**0.46%**	**0.51**
TREE	40.12%	**40.93%**	50.65%	**49.47%**	**50.59%**
TREO*	46.98%	**47.93%**	59.31%	**57.93%**	**59.24%**
Th	0.61%	**0.35%**	1.14%	**0.43%**	**0.45%**
U	0.04%	**0.01%**	0.03%	**0.01%**	**0.01%**
Specific Activity Bq/g	29.7	**15.4**	50.0	**18.7**	**19.5**

13.6.3 Specific activity

The radioactivity of the concentrate, known as the specific activity, is measured in Becquerels per gramme, Bq/g, calculated using the Th and U grades. Bq/g values can be measured directly by gamma spectroscopy or determined based on elemental analysis for Th and U (41 Bq/g for every 1% Th plus 125 Bq/g for every 1% U).

The monazite concentrate created by SGS during the metallurgical testing has a specific activity of 18.7 Bq/g according to the more accurate Actlabs assays. Based on the EPMA values, pure Eureka monazite has a specific activity of 26.6 Bq/g, so it is not likely that the Eureka monazite concentrate would exceed 27 Bq/g.

Material below 10 Bq/g is exempt from radioactive transport regulations as outlined by the International Atomic Energy Agency ("IAEA") and can be shipped as general cargo. Material above this level is "Class 7" and must be transported according to international and national regulations as outlined by the IAEA.

13.6.4 Dose rate measurement

For Class 7 shipments, customs officials typically test the ionizing radiation dose-rate at the external surface of packaged material; this is measured in microsieverts per hour ("μSv/h"). This measurement scale is partly dependent on specific activity and partly dependent on radionuclide chemistry and the shielding effect of packaging.

Class 7 material measuring below 5 μSv/h is considered an "Excepted Package" under the low risk applicable code UN 2910. The regulatory requirements are simplified for UN2910 to reflect the low risk of this material. Goods with surface dose-rate values above 5 μSv/h are classed as UN2912 and are subject to stricter regulations.

E-Tech Namibia measured the dose rate emanating from the monazite concentrate stored in a glass container (seen in Figure 13-6) and recorded a value of 3.5 μSv/h. Whilst this is encouraging it is not known how this would change according to different container materials and larger consignment volumes.

If necessary, there are options to reduce the detectable dose rate, firstly by using a substantial container such as a steel drum rather than plastic materials. Secondly there is the option to blend magnetite into the concentrate to bring the Th and U grades down, thereby lowering specific activity; magnetite can then easily be removed after shipping by dry magnetic separation.

Some of the key differences between UN 2910 and UN 2912 are outlined in Table 13-6 below.

Table 13-6: IAEA guidance for transporting NORM

UN2910	UN2912
May contain and be transported with other goods.	The package may not contain any items other than those that are necessary for the use of the radioactive material
Must be packaged.	May be transported unpackaged under "*Exclusive Use*".
The radiation level at any point on the external surface of an excepted package may not exceed 5 μSv/h.	The maximum radiation level at any point on any external surface of the package or overpack may not exceed 2 mSv/h (note alternatives and exceptions).
Transport Index (TI) tri-foil **not** required.	Transport Index (TI) tri-foil type to be determined. packages and overpacks are assigned to category IWHITE, category II-YELLOW or category III-YELLOW.
Mark each package with "UN 2910".	Mark each package with "UN 2912" and "RADIOACTIVE MATERIAL, LOW SPECIFIC ACTIVITY (LSA-I)". Also mark each package that conforms to an IP-1 design with "TYPE IP-1".
Marking with the word "RADIOACTIVE" on an internal surface in such a manner that a warning of the presence of radioactive material is visible on opening the package.	Labels must be fixed to two opposite sides of the outside of the package or overpack, or on all four sides of a freight container. Mark the label with the contents "LSA-I" and the maximum activity of the contents (in MBq or GBq).
May be sent by domestic and international shipping.	Various restrictions and requirements to be implemented during transport and shipping.

13.7 SRK Comments

The SGS testwork programme, described by SGS as “scoping”, resulted in the production of a concentrate containing 59% TREO at a recovery rate of between 60% (Sm) and 69% (Pr), with the recovery of Ce, La and Nd averaging 65%, the same recovery as reported for P_2O_5, which was used in the testwork as the proxy for monazite. Recovery was by gravity separation with magnetic separation used for magnetite removal as a finishing stage.

SGS notes that there is potential to improve recovery by treating the middlings and tailings streams from the gravity separation stage, possibly with further grinding and/or using a combination of gravity separation and flotation and SRK endorses this view.

Further upgrading of the gravity concentrate by gravity separation and/or flotation, with or without regrinding, may have the potential to increase the TREO grade of the concentrate, albeit likely at the expense of recovery. Reprocessing of the tailings from such upgrading stages would therefore be required in order to attempt to achieve further recovery without compromising grade.

Further testwork will therefore be required to:

- optimise the process route;
- determine the optimum TREO concentrate grade, recovery and mass yield;
- assess and quantify the variability in metallurgical response across the deposit; and
- determine the costs and benefits associated with dose rate control measures if necessary.

14 MINERAL RESOURCE ESTIMATION

14.1 Introduction

The geological modelling was undertaken by Impala using Leapfrog Geo software and the block modelling was undertaken by Baker Geological Services. Both processes were completed in Q2 2020 and both have been reviewed by SRK. SRK also performed spot checks of the database against digital assay certificates, determined an appropriate cut-off grade, made an assessment of reasonable prospects for eventual economic extraction, and reported the Mineral Resource in accordance with the JORC Code.

14.2 Mineralisation Wireframes

Impala created a geological model based on the lithological logging in trenches and RC drillholes, spectral gamma logging, surface mapping and assay data resulting in 14 distinct carbonatite dyke wireframes reflecting the mapped surface expression and extrapolated to 75 m below surface based on drillhole intersections. In certain situations, where drilling and trenching data has not been collected yet, or is limited (particularly in zones 3 and 4), wireframes for mapped carbonatite dykes have been constructed based on surface mapping data only, with the dip aligned to surface structural measurements and thicknesses assigned from the surface mapping. These unsampled dykes have been constructed for exploration and planning purposes and do not form part of the Mineral Resource estimate.

The mineralisation wireframes have been clipped to a topographic surface constructed from drone stereographic aerial imagery with an average accuracy of 0.1 m.

Due to the limited extent of surface weathering and cover, no weathering wireframes have been created for the Project.

Table 14-1 lists the domains that were created.

Table 14-1: Modelling Domains and Estimation Zone codes

Domain	Zone
1A	10
1B	11
1C	12
1D	13
1E	14
1F	15
1H	17
2A	20
3A	30
3B	31
3C	32
3D	33
3E	34
3MC	35

A plan map showing the estimation domain wireframes is presented below in Figure 14-1 and a cross section through the wireframes is shown in Figure 14-2.

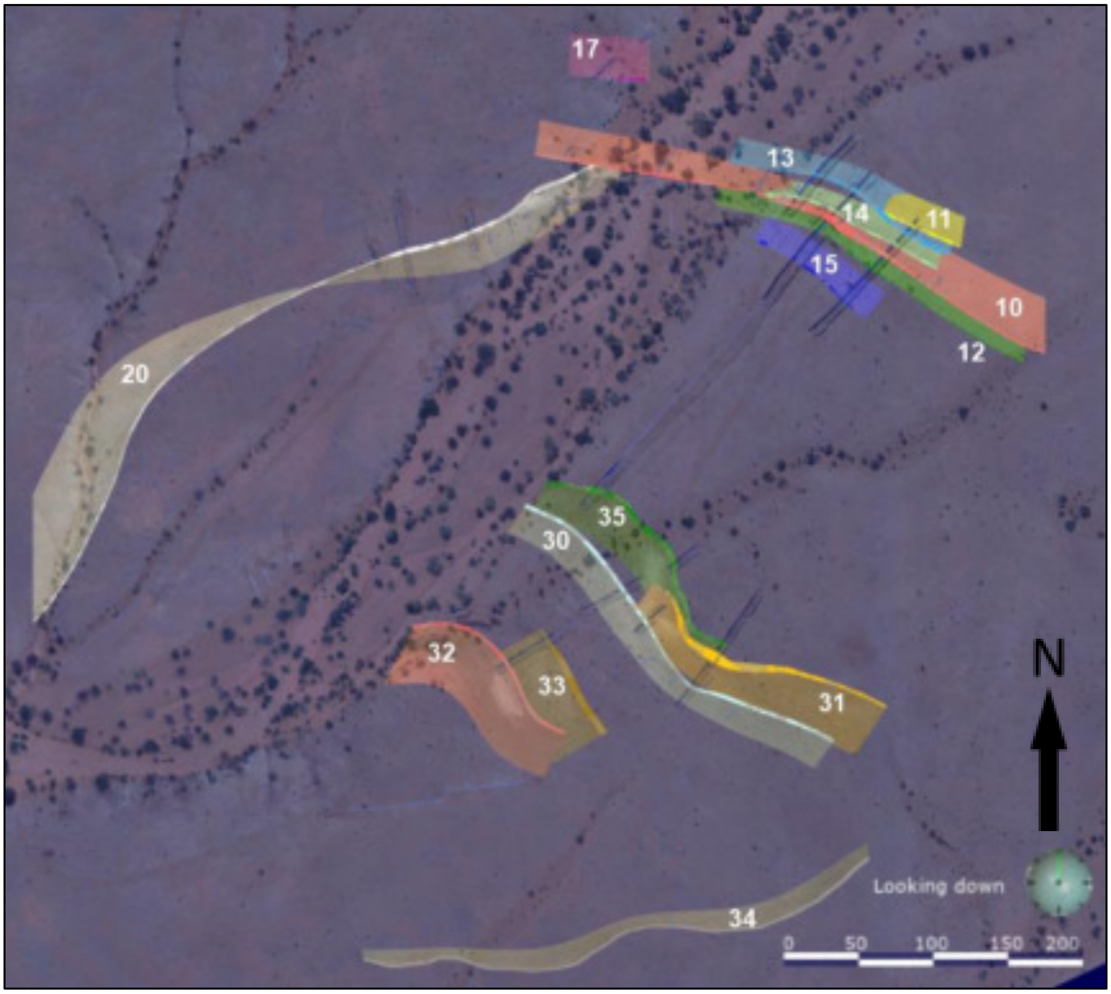

Figure 14-1: Plan map of mineralisation wireframes and estimation domain codes

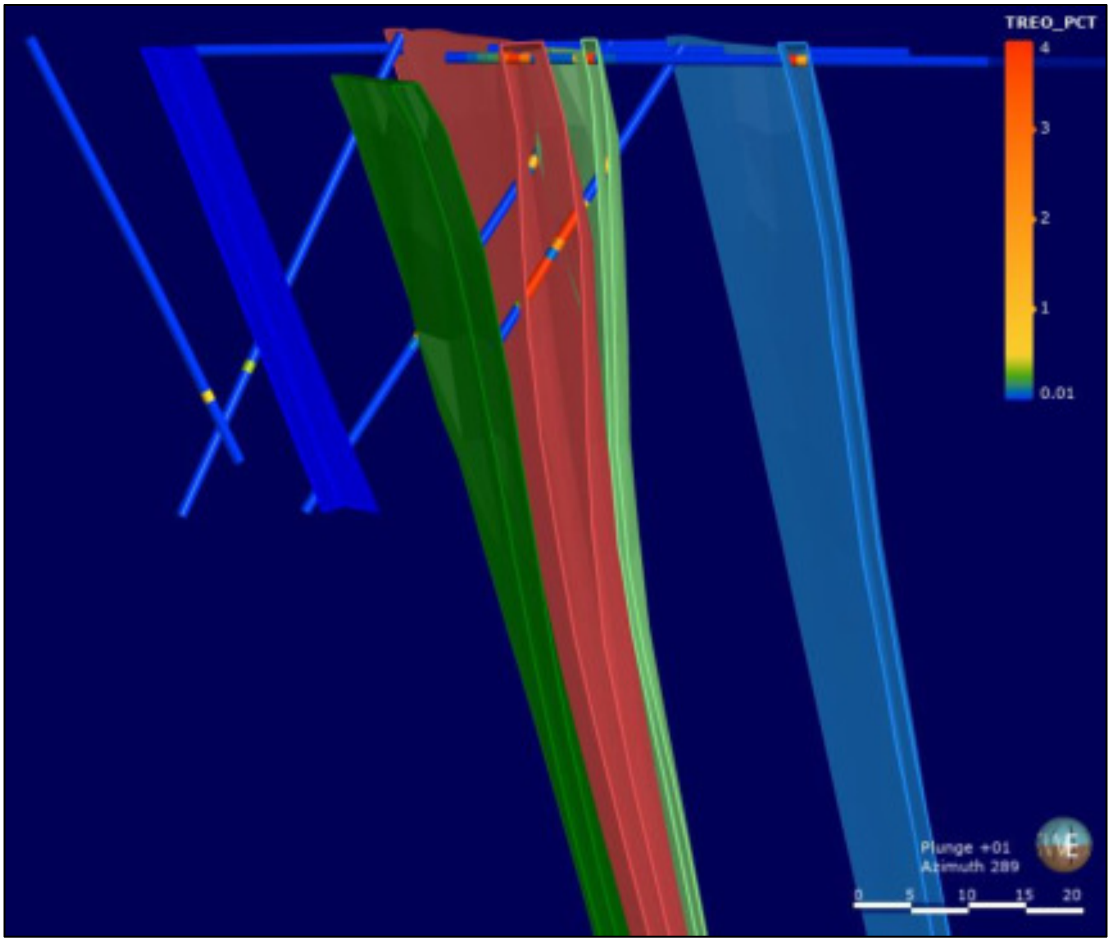

Figure 14-2: Cross Section through mineralisation wireframes

14.3 Statistical Analysis

14.3.1 Introduction

This section presents the results of the statistical studies undertaken on the available assay data to determine their suitability for use in the Mineral Resource estimation process and to establish suitable block model grade estimation parameters.

14.3.2 Compositing

Data compositing is often undertaken to regularise sample lengths and thus remove bias, and to generate sample sizes appropriate to the scale and methods of the mining operation envisaged.

Given the limited amount of data at this stage of the Project, the consistent sample length and the relatively thin and steeply dipping nature of the host dykes, it was decided to work with the raw sample interval length of 1 m. No compositing was therefore required.

14.3.3 Zone statistics

Figure 14-3 shows histogram of %TREO encompassing all of the samples in all of the mineralisation zones (a total of 161 samples) and which have a mean grade of 3.3% TREO.

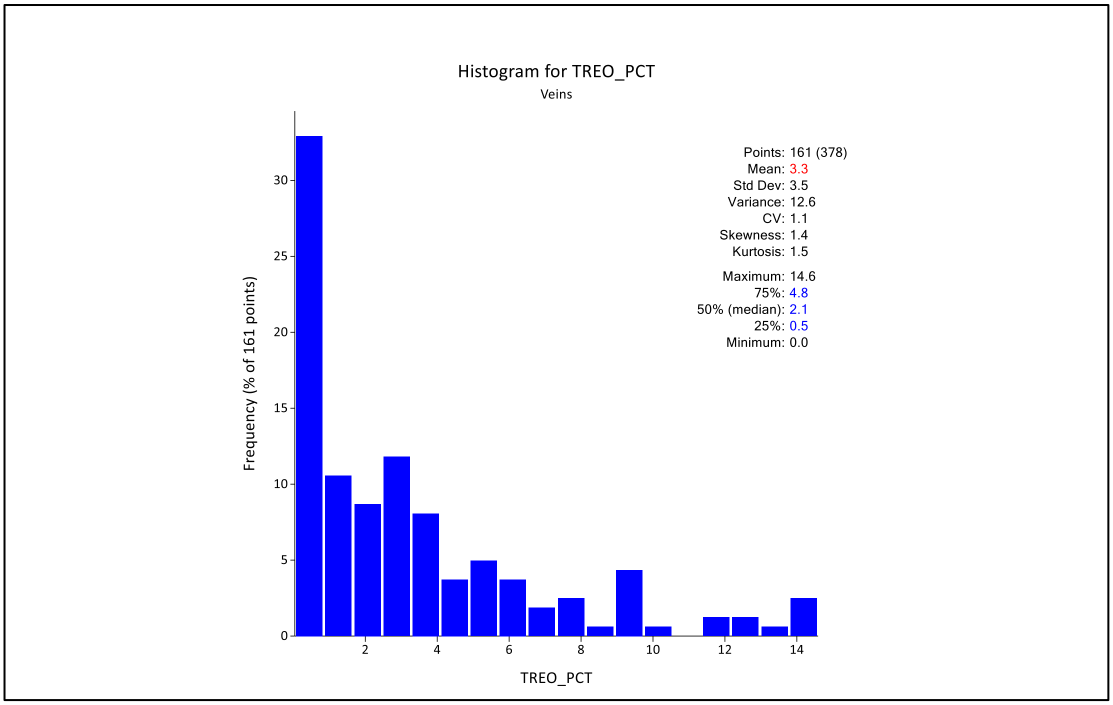

Figure 14-3: Eureka combined zone TREO% histogram (Source: BGS)

It is noted that the LREO's (La_2O_3, Ce_2O_3, Pr_2O_3, Nd_2O_3 and Sm_2O_3) make up over 99% of the TREO with the HREO component making 0.39% of the TREO. Figure 14-4 shows a pie chart for the highest grade Estimation Zone 10.

Figure 14-5 shows the scatterplots of each LREO against the TREO%. As shown, all LREO's have a strong correlation with TREO%. Given that over 99% of the REO fall within the LREO category, the scatterplots of HREO and TREO% has not been shown.

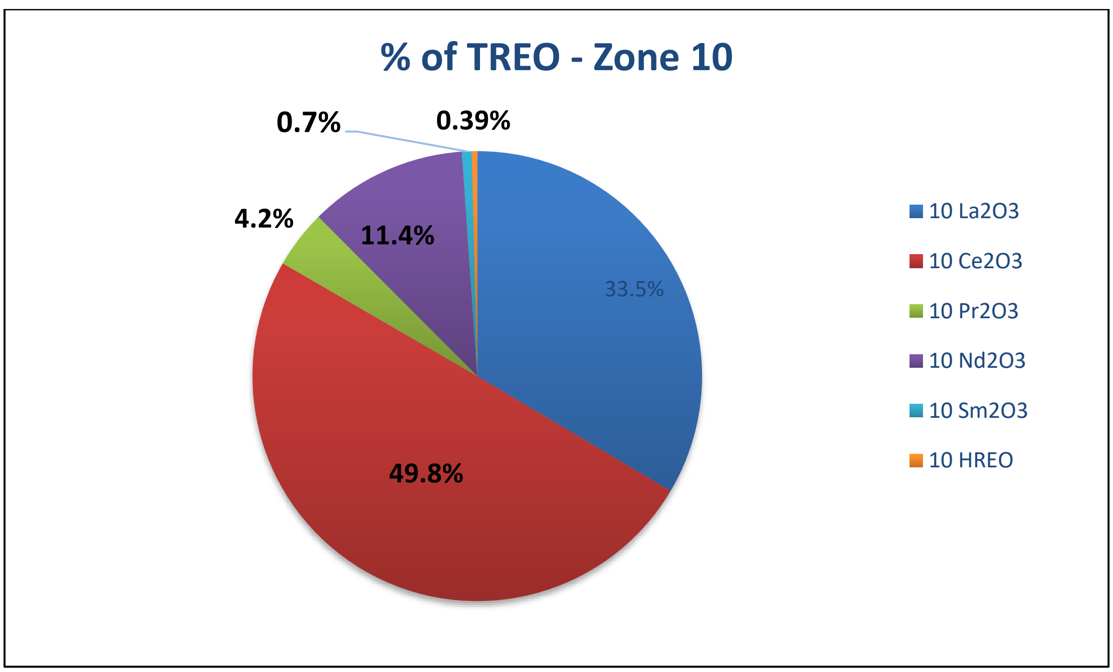

Figure 14-4: Eureka zone 10 pie chart (Source: BGS)

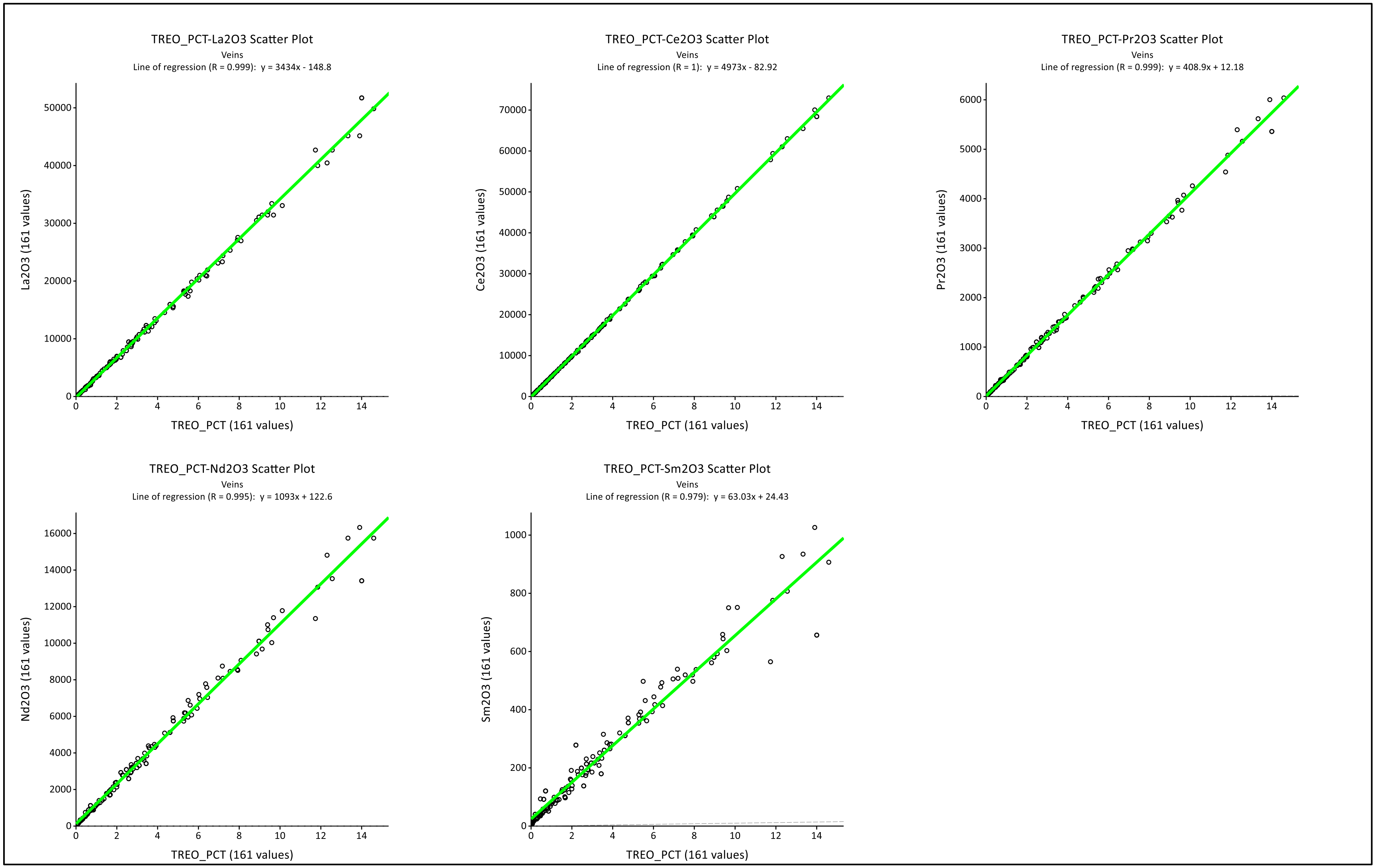

Figure 14-5: Eureka zone LREO% Scatterplot against TREO% (Source: BGS)

14.4 Density Analysis

Due to an absence of appropriate sample material, systematic density measurements have not yet been undertaken for the Project. Density measurements have however been made on surface grab samples of fresh carbonatite, which provide a reasonable representation of mineralised carbonatite and waste rock. During the metallurgical testwork a total of 10 density measurements were also made using the water immersion displacement method. Subsequently, a further 18 carbonatite and 3 waste rock grab samples were collected from surface outcrops for density analysis using the same method. The samples of fresh carbonatite and waste rock are not considered porous or vuggy enough to warrant coating or wrapping prior to immersion). Each of the grab samples were then submitted for assay at Wheal Jane Laboratory (UK) and analysed for Ce and P via ICP-OES to allow a linear regression between Ce and density to be established. Images of the density measurements being taken are provided in Figure 14-6 below.

Figure 14-6: Density sampling of surface mineralised grab samples

Density has been applied to the model using a regression equation which relates Ce ppm to the measured density. Table 14-2 shows the regression formula which is based on the best fit line shown in Figure 14-7.

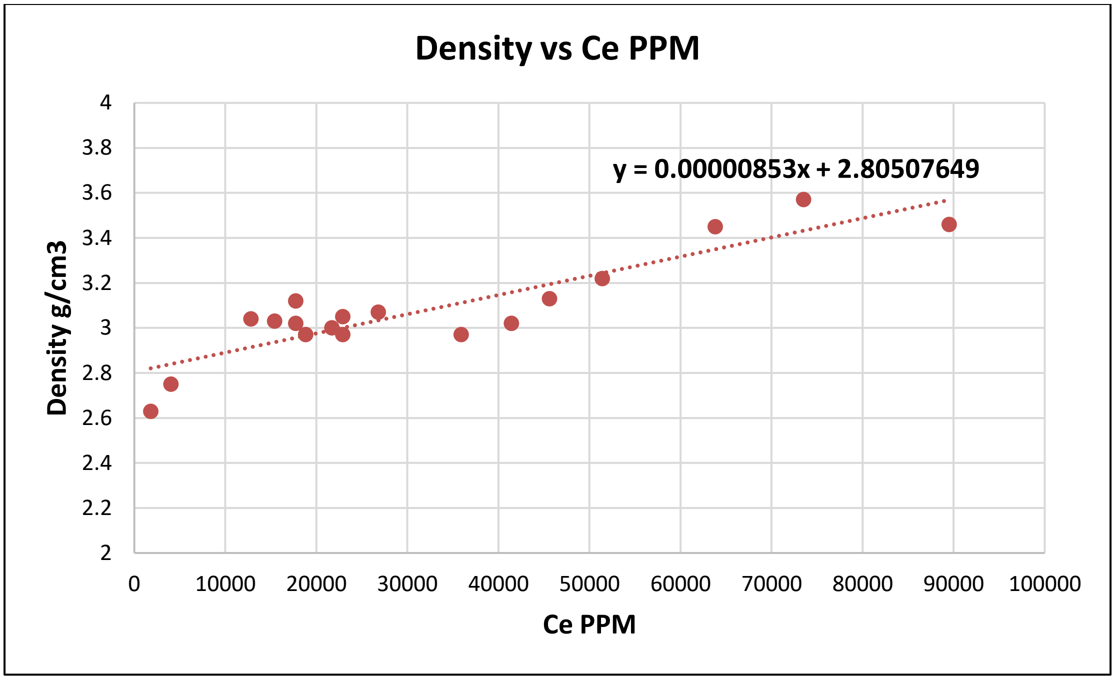

Figure 14-7: Density vs Ce PPM (Source: BGS)

Table 14-2: Eureka density regression formula

Variable	Regression Formula
Ce ppm	CEDEN=(0.00000853*Ce) + 2.80507649

14.5 Geostatistical Study

Given the limited amount of data, directional variography by domain was not possible. For the geostatistical study, all zones were therefore combined and experimental omni-directional variograms run on the TREO % and P_2O_5 % assays only. The omni-directional variograms were created using the 1 m composite drillhole file.

Despite the low levels of data, the omni-directional variograms showed a reasonable structure. A two-structure modelled line of best fit was possible with a total range of 44 m. The same variogram model was used to fit the TREO and P_2O_5 experimental variograms. The variograms enabled Ordinary Kriging ("OK") to be used as the interpolation technique which then allows the estimation quality to be assessed through further studies.

Figure 14-8 and Figure 14-9 show the combined zone omni-directional variograms for TREO and P_2O_5, respectively.

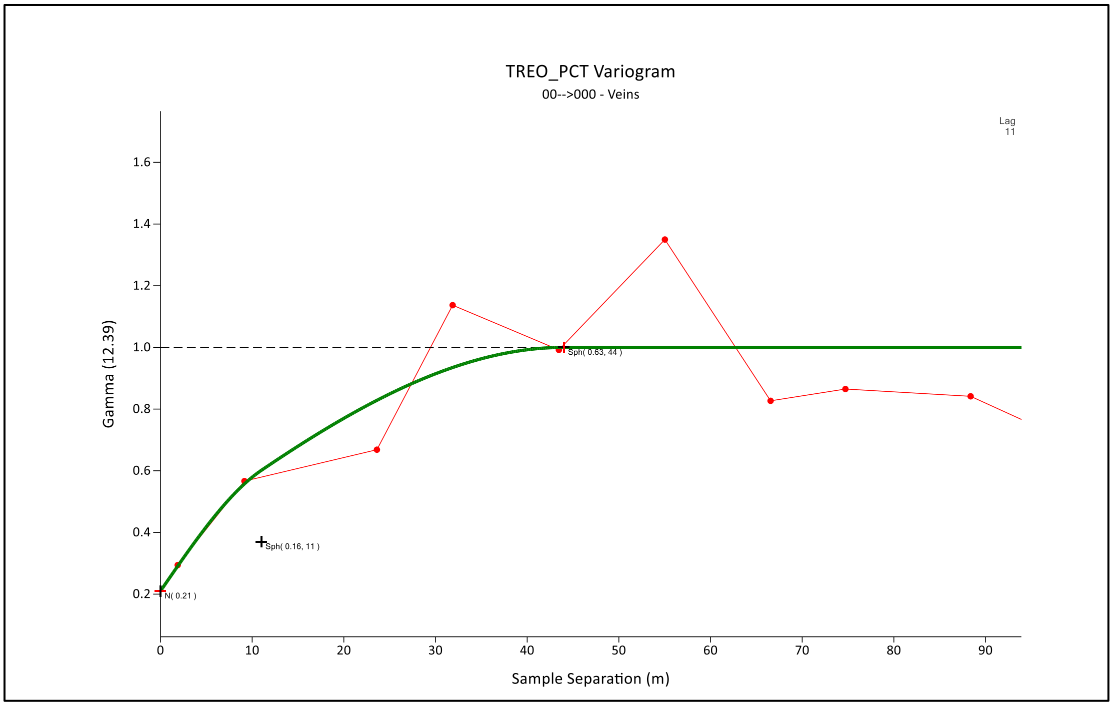

Figure 14-8: Eureka combined zone omni-directional variogram – TREO% (Source: BGS)

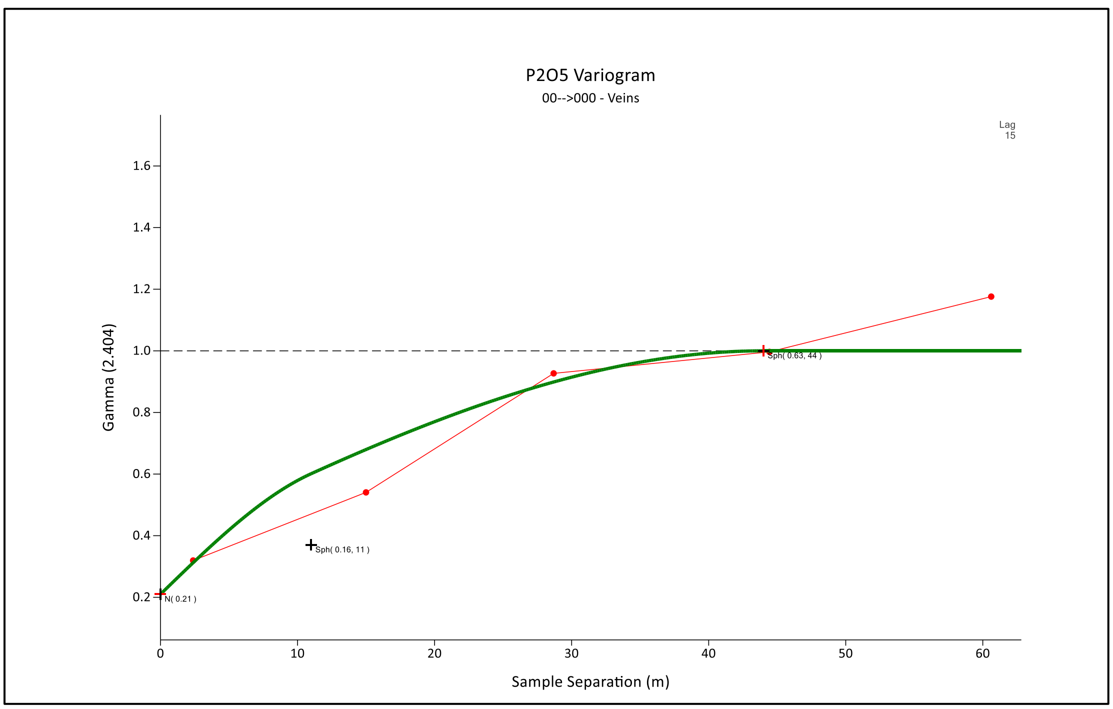

Figure 14-9: Eureka combined zone omni-directional variogram – P_2O_5% (Source: BGS)

The results of the variography were used to assign the appropriate weighting parameters to the sample pairs utilised to inform the block model grade.

The total range modelled is also incorporated to help define the optimum search parameters and the search ellipse radii dimensions used in the interpolation. Ideally, sample pairs that fall within the range of the variogram (where a strong covariance exists between the sample pairs) should be utilised if the data allows.

The results of the variography suggest that Ordinary Kriging ("OK") is an appropriate interpolation technique despite the limited sample support.

14.6 Interpolation Parameters

The interpolation parameters were selected following a visual assessment of the sample support. Numerous interpolation runs were undertaken using varying parameters with the estimates completed being validated after each run. This process resulted in the parameters shown in Table 14-3 to Table 14-5 being used for each estimation run.

All zones used an isotropic search with Run 1 adopting a search radius of 50 m with a minimum of 4 samples and a maximum number of 10 samples required to estimate the block grade. A maximum of 2 samples were allowed from a single drillhole, effectively forcing the search ellipse to use at least 2 drillholes in the estimate should the minimum of 4 samples be used. For the estimate to use 10 samples in the grade estimate, 5 drillholes would be required. Run 2 captured blocks not estimated into by Run 1 using a larger search ellipse and Run 3 ensured the rest of the blocks were all estimated by using a larger range and lower minimal number of samples. The first pass search ellipse applied at Eureka is shown in Figure 14-10.

Table 14-3: Run 1 Interpolation Parameters

Zone	Ellipse range X	Ellipse range Y	Ellipse range Z	Angle 1	Angle 2	Angle 3	Min Samples	Max Samples	Max Samples per Drillhole
All	50	50	50	0	0	0	4	10	2

Table 14-4: Run 2 Interpolation Parameters

Zone	Ellipse range X	Ellipse range Y	Ellipse range Z	Angle 1	Angle 2	Angle 3	Min Samples	Max Samples	Max Samples per Drillhole
All	100	100	100	0	0	0	4	10	2

Table 14-5: Run 3 Interpolation Parameters (estimates all blocks not estimated after Run 1 and Run 2)

Zone	Ellipse range X	Ellipse range Y	Ellipse range Z	Angle 1	Angle 2	Angle 3	Min Samples	Max Samples	Max Samples per Drillhole
All	500	500	500	0	0	0	2	10	2

14.7 Block Modelling

14.7.1 Block model parameters

The block model was created using a parent cell block size of 10 mY by 10 mX by 5 mZ with sub-cells used to a minimum size of 0.5 mX x 0.5 mY x 0.5 mZ. A small sub-cell size was deemed appropriate due to the thin nature of the mineralised dykes and the requirement to honour the contacts and maintain an accurate volume. Table 14-6 summarises the block model parameters.

Table 14-6: Block Model Framework

	ORIGIN	MAX	DISTANCE	SIZE	BLOCKS
X	525750	526600	850	10	85
Y	7561950	7562750	800	10	80
Z	1005	1110	105	5	21

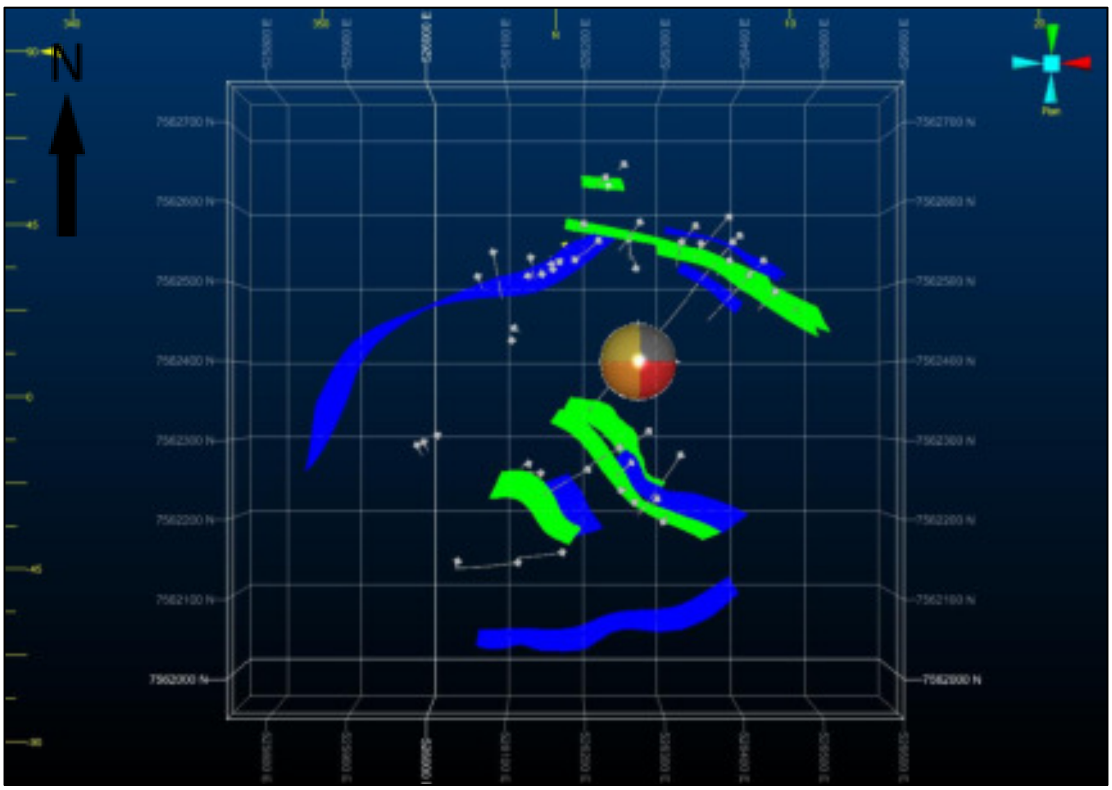

Figure 14-10: Eureka 50 m x 50 m isotropic search ellipse (Source: BGS)

14.7.2 Grade interpolation

Grades of TREO%, P_2O_5, Th, U, La, Ce, Pr, Nd, Sm, Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb, Lu, Sc and Y were interpolated into the empty block model using OK and the interpolation parameters based on the results of geostatistical study. A three-pass approach was used to ensure themajority of blocks were estimated in estimation runs 1 and 2 using an isotropic search ellipse dimension of half the geostatistical range (50 m) and at the geostatistical range (100 m) respectively; a larger third search ensured all blocks within the estimation domains were assigned a grade.

Individual REE element grades were subsequently converted to REO grades using the conversion factors given in Table 11-3.

Post estimation processes included the following:

- Slope of Regression calculation to enable an assessment of the quality of the estimate;
- Conversion of all REE to oxides;
- Calculation of the combined LREOs; and
- Calculation of the combined HREOs.

Figure 14-11 shows the block model coloured by the estimation pass with the green blocks being those captured by Run 1, the orange blocks being those additional blocks captured by Run 2 and the red blocks being those final blocks only captured by Run 3. The white blocks were not interpolated into by any run. Figure 14-11 clearly shows that the Run 1 estimate captures most of the block model area supported by drillholes and the Run 2 estimate is more distant from the samples therefore carrying a higher risk in terms of estimation accuracy.

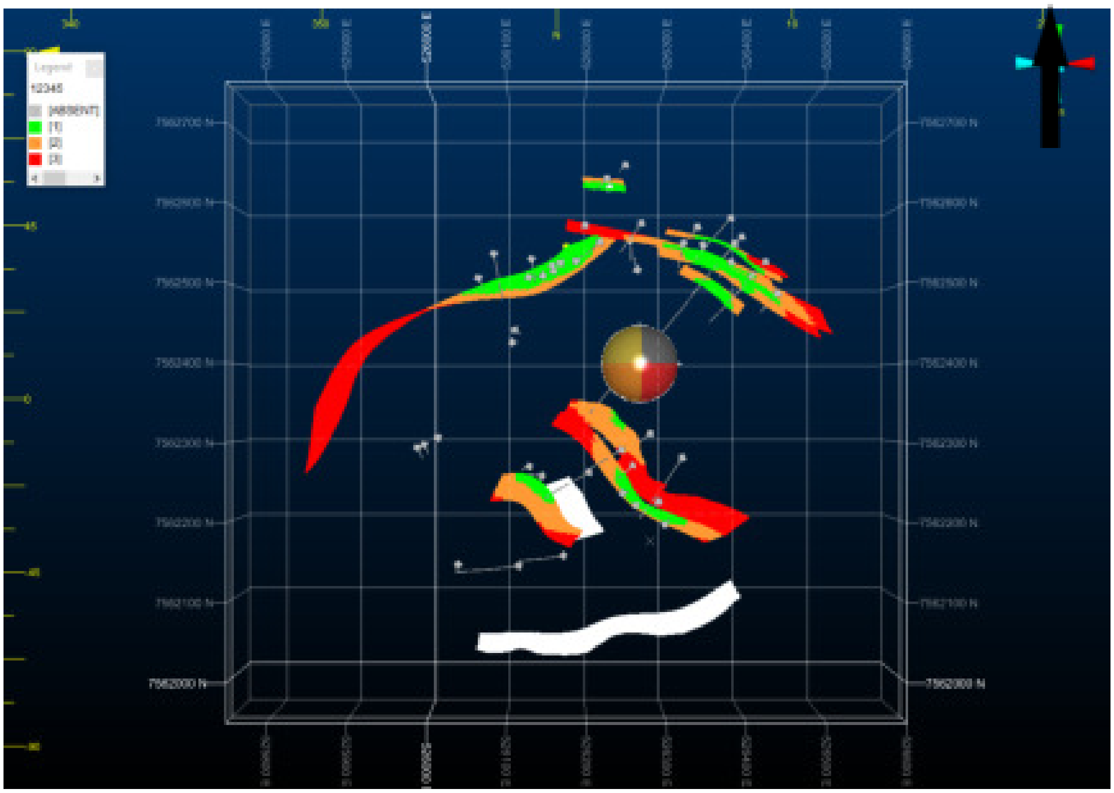

Figure 14-11: Eureka Block Model Estimation Run, (Source: BGS)

14.7.3 Drillhole count

The average number of drillholes used to estimate the block grades was determined per zone; zones 10, 12, 13, 20 and 30 used between 4 and 5 drillholes with other zones using fewer drillholes.

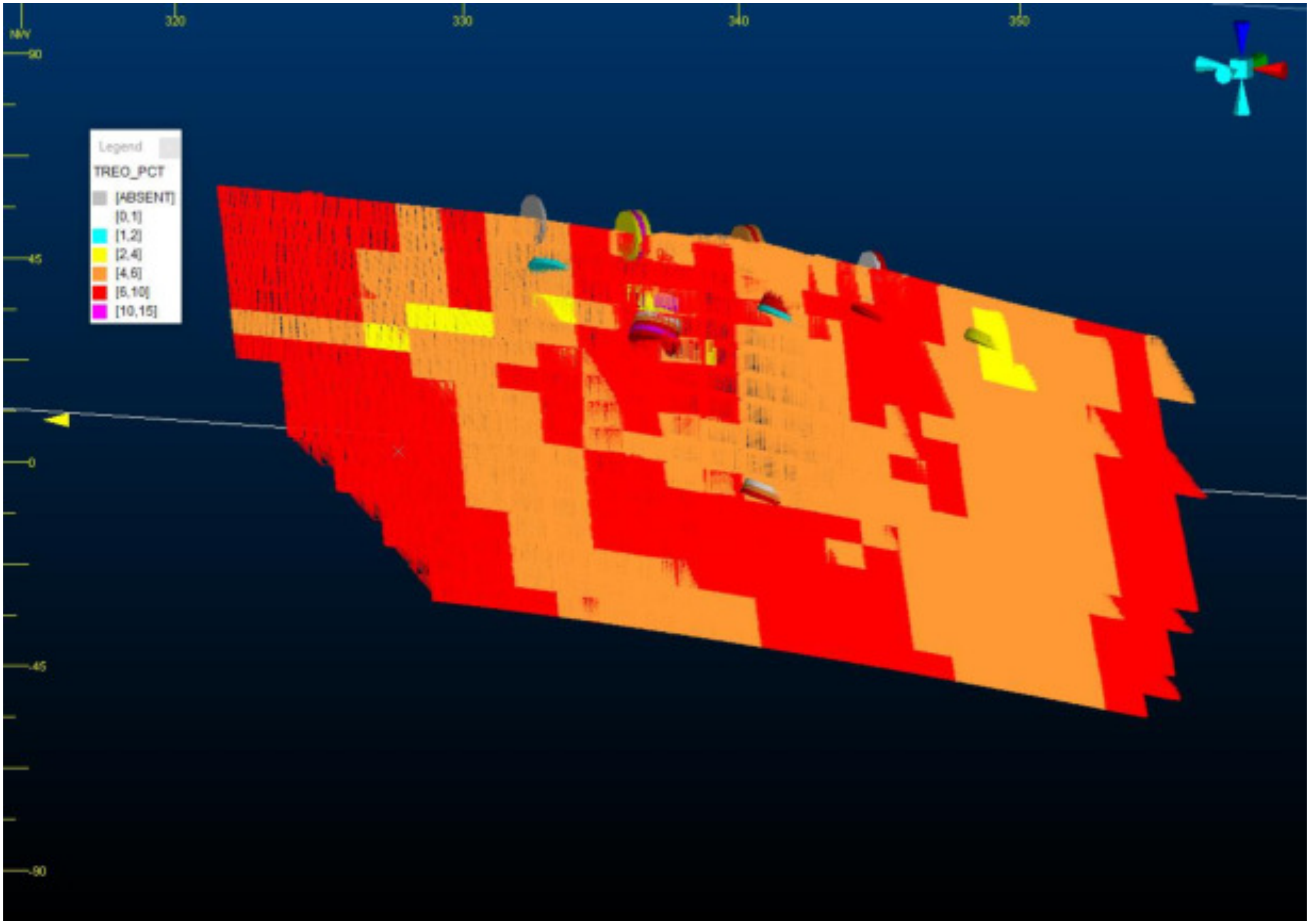

Figure 14-12: Eureka Block Model : visual validation of block grades in zone 10 pass 1 or 2 (Source: BGS)

14.8 Block model validation

The block model has been validated using the following techniques:

- visual inspection of block grades in plan and section and comparison with drillhole grades;
- comparison of global mean block grades and sample grades within mineralised zones; and
- a review of the slope of regression.

14.8.1 Visual Validation

Figure 14-12 shows an example of the visual validation checks highlighting the reasonable correspondence between the block TREO% grades and the sample TREO% grades. That said, it is acknowledged that the low levels of data support generally restricts the quality of the estimated grade distribution.

14.8.2 Global mean comparison

A comparison of the block mean grades and the composite sample means of TREO is provided in Table 14-7. This was only completed on those blocks that were estimated in Run 1 of the estimation as it has been shown that Run 1 effectively estimates the grades surrounding the drillhole data and that Runs 2 and 3 are lower confidence estimates whereby a larger search ellipse is required and those blocks estimated in Runs 2 and 3 are clearly more distant from the drillhole samples. The difference between sample grades and block grades is due to clustering of drillhole intersection locations and also the localisation of the block grade estimate, differences are tolerably small in most domains higher in others indicating the need for better drilling coverage to improve confidence in the grade estimation in future.

Table 14-7: Block Grade vs Sample Grade

ZONE	Field / Unit	No. Of Composite Samples	Block Model Mean – Run 1	Composite Mean	Absolute Difference	Relative Difference
10	TREO %	33	6.17	6.01	-0.16	3%
12	TREO %	12	3.14	2.53	-0.62	20%
13	TREO %	13	5.11	4.21	-0.9	18%
14	TREO %	8	2.11	2.28	0.17	8%
15	TREO %	5	8.96	9.32	0.36	4%
17	TREO %	6	1.67	1.7	0.04	2%
20	TREO %	33	2.59	3.16	0.57	22%
30	TREO %	17	1.84	2	0.16	9%
32	TREO %	8	0.74	1.86	1.12	152%
35	TREO %	13	0.35	0.32	-0.03	10%

Slope of Regression

The slope of regression can be used as a guide to assess the quality of the grade estimate; a value approaching 1 being deemed a high-quality estimate. Table 14-8 shows the mean slope of regression values for those blocks estimated in Run 1. As shown the mean values are relatively low with the highest mean recorded in zone 10.

Table 14-8: Eureka slope of regression by zone (Run 1 only)

ZONE	FIELD	MINIMUM	MAXIMUM	MEAN
10	TREO_SL	0.00	0.93	0.56
12	TREO_SL	0.00	0.80	0.42
13	TREO_SL	0.00	0.86	0.35
14	TREO_SL	0.00	0.89	0.41
15	TREO_SL	0.00	0.75	0.35
17	TREO_SL	0.00	0.78	0.26
20	TREO_SL	0.00	0.92	0.42
30	TREO_SL	0.00	0.89	0.43
32	TREO_SL	0.00	0.79	0.35
35	TREO_SL	0.00	0.23	0.07

Figure 14-13 shows the distribution of blocks coloured by the Run 1 slope of regression where it is clear that higher values are clustered around the drillhole data with the slope of regression reducing significantly, even within the Run 1 estimate as the blocks become more distant from the samples.

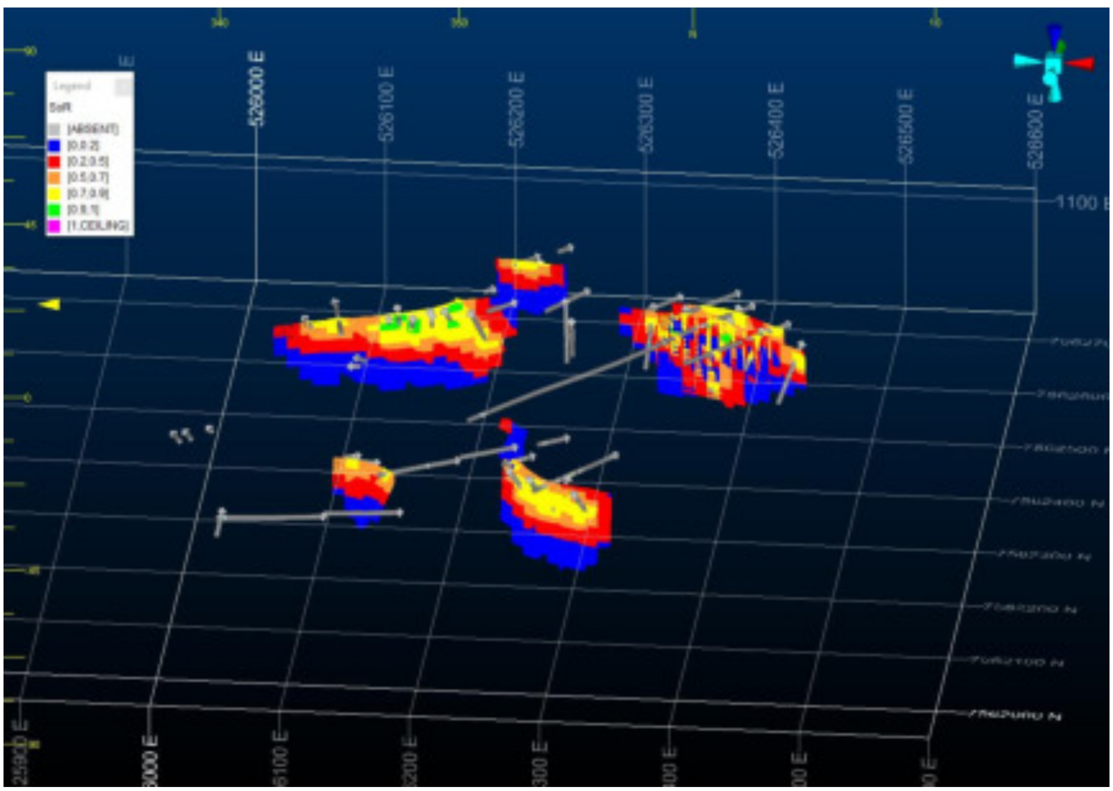

Figure 14-13: Eureka Slope of Regression for the Run 1 estimate (Source: BGS)

Tonnage Estimation

As discussed in Section 14.4, a variable density value has been determined based on the Ce assay value to reflect the influence that the dense mineral monazite has on the density of the carbonatite. The regression was applied to all blocks upon completion of the grade estimate. Table 14-9 shows the average calculated average for each zone.

Table 14-9: Eureka average density by zone

ZONE	DENSITY
10	3.02
11	2.83
12	2.92
13	2.98
14	2.87
15	3.12
17	2.86
20	2.88
30	2.87
31	2.83
32	2.83
33	2.89
34	2.89
35	2.82

14.9 Classification

In SRK's opinion, the trench and drillhole sampling is of sufficient quality and coverage to enable the reporting of an Inferred Mineral Resource in many areas. However, several parts of the model particularly at depth are based on considerable extrapolation of surface mapping and trenching or are informed by relatively wide spaced drilling. In SRK's opinion these areas require better definition before being reported as a Mineral Resource.

Specifically, SRK has limited the Inferred Mineral Resource to a 50 m extrapolation beyond trenching and drilling intersections and surface mapping where this is available to support the sampled parts of the model. This distance reflects the many dykes which have multiple observation points demonstrating strike continuity over at least 100m.

The RC drilling method limits the accuracy with which dyke thickness can be assessed due to the fixed 1m sampling arrangement. Given the thin nature of the dykes in many places and the small-scale mining approach therefore needed to achieve good selectivity, SRK considers it important to improve the accuracy of dyke thickness determinations with diamond core drilling before the model is ready to use for mine planning.

The RC drilling method also is also prone to grade smearing between adjacent samples and loss of fines which may introduce a sampling bias. This is another reason to limit the classification to 'Inferred' (rather than the higher confidence categories of 'Indicated' and 'Measured') at this time. Good quality diamond drilling will overcome this concern and also provide much more accurate dyke geometry information as well as samples that can be used for comminution testwork.

SRK considers it will be necessary to infill the drilling coverage to achieve better than 30 m drill spacing horizontally and vertically so that localised geometrical features and high or low grade areas within the dykes with can be determined with better confidence.

The assaying QAQC should be continued and ideally improved with more relevant grade CRMs to make the assessment of laboratory accuracy much more robust. It may also become important to introduce CRMs for thorium assay determinations so that the premise of a constant ratio of dose rate to TREO can be demonstrated with high confidence.

The density determinations provide a reasonable basis for tonnage estimation although with core drilling in the future there will be the opportunity to increase the number of density determinations to improve confidence.

Part of the resource in the vicinity of T026 has not been influenced by the low grade encountered in the trench, this area has not been included in the Mineral Resource. SRK has further limited the Inferred Mineral Resource to a pit shell derived using optimistic input parameters, so as to capture mineralisation with reasonable prospects of being mined economically in addition to that which would be economical today so reflecting the requirements of a Mineral Resource as detailed in Section 14.10.2.

14.10 Mineral Resource Reporting

14.10.1 Introduction

In order to determine a suitable reporting cut-off grade and to assess the reasonable prospects for eventual economic extraction, a pit optimisation exercise has been undertaken by SRK. This has been based on technical-economic parameters derived from comparable projects and typical costs for the types of processes currently envisaged. It is important to understand that beyond the metallurgical testwork described in Section 12, no dedicated technical-economic studies have yet been completed for Eureka. The numbers presented in this ITR are therefore provisional and approximate estimates which SRK considers reasonable for the purposes of reporting Mineral Resources. Notably, revenue parameters are based on current REO prices and an assessment of discount rates currently prevailing in the industry.

All the pit optimisation parameters presented in this report are conceptual, have been derived purely for the purpose of limiting the Mineral Resource to mineralisation with reasonable prospects for eventual economic extraction, and are subject to change following more detailed work that will be undertaken as part of future technical studies.

14.10.2 Pit Optimisation parameters

It is assumed that mining will be by open pit, with conventional truck and excavator mining methods, focussing on selective extraction, rather than particularly high production rates, to minimise dilution of the mineralised carbonatite dykes with waste rock. For the purpose of pit optimisation, the sub-blocked model was regularised to 1 x 1 x 1 m cubes which had the effect of incorporating dilution which likely to be incurred despite fine-scale mining selectivity.

Operating Costs

A mining cost of 5 USD per tonne moved has been used when considering cut-off grade and pit optimisation parameters. This is at the upper end of typical open pit mining costs in Africa reflecting the low assumed total mining rate of approximately 3 Mt per annum.

Concentration of the monazite is expected to be achieved using simple gravity and magnetic processes, as demonstrated by metallurgical test work described in Section 13.2. The testwork was a first pass assessment which achieved a 65% TREO recovery, a mass pull of 10% and a concentrate grade of 59% TREO. SRK considerers it reasonable that with further mineral processing testwork, recovery might improve to a 70% recovery and this has been used when considering cut-off grade and pit optimisation parameters. At this stage the concentrate production rate is provisionally expected to be approximately 400 to 500 tonnes per month.

The gravity plant is likely to consist of a primary jaw crusher, secondary cone crusher, screens, spirals, jigs and shaking tables. A low intensity magnetic separator ("LIMS") can also be added to the processing circuit if magnetite separation from the monazite concentrate is desirable. A provisional processing cost of 25 USD per tonne milled is considered reasonable in the absence of any specific cost estimate; this is the most significant component of operating costs and has been used when considering cut-off grade and pit optimisation parameters.

General and Administrative costs are estimated at 6 USD per milled tonne and an additional allowance of 7 USD per tonne of concentrate has been made to cover the 140 km road haul from the mine to Walvis Bay and likely port handling fees.

A pit slope of 55 degrees has been used to reflect the competent nature of the host rocks as evidenced at the nearby Navachab gold mine.

Concentrate Price Determination

E-Tech Namibia's concept for the Eureka Project is to produce a monazite concentrate and to ship this from Walvis Bay to traders, refiners and/or end-use customers. Further downstream refining will be undertaken by other parties and therefore the price paid to the Eureka Project owners per tonne of concentrate will be at a discount to the theoretical market value of the contained individual Rare Earth Oxide ("REO") amounts.

The mineral concentrate price depends on:

- the average market price of the individual REOs weighted by their proportion in the TREO grade known as the "basket" price;
- the TREO grade of the concentrate;
- a payability reduction, typically discounting by 60-70% to reflect the downstream costs for the end buyer to produce separated pure REO products on which basis market prices are reported; and
- further discounts for impurities and complex mineralogy may also be applied.

E-Tech Namibia has based its expected concentrate value calculation on the main value drivers experienced by Rainbow Rare Earth's (LSE:RBW) ("RBW") Gakara Project in Burundi. Gakara has stockworks of narrow, high-grade veins of almost pure bastnäsite and monazite; the ore requires minimal treatment achieve the 54% TREO grade required for export and sale. The resulting concentrate comprises both bastnäsite and monazite, two chemically different REE minerals.

RBW has an offtake agreement in place with Thyssenkrupp Materials Trading ("TK") for its rare earth concentrate; the price paid for its mineral concentrate is based on the prevailing market "basket" price of the contained REEs less an overall discount. The current discount rate is approximately 70% and may vary depending on the arrangements TK negotiates with new customers or renegotiates with existing customers.

The Eureka mineral concentrate TREO basket, like that of RBW, is weighted towards the light REOs and SRK considers it reasonable to assume the concentrate would be priced on a similar basis. However, the mono-mineralic nature of the Eureka concentrate (monazite only) is likely to make the downstream process less costly which may therefore result in a lower discount factor. Furthermore the TREO grade of the Eureka concentrate is likely to be closer to 59% higher than the 54% achieved by RBW which would similarly be expected to attract a lower discount factor.

On this basis E-Tech Namibia assumes a 60% discount factor will be applied to the basket value of the TREO contained in concentrate, compared with the 70% discount applied to the RBW concentrate.

A breakdown of REO proportions for the Eureka TREO "basket" is provided in Figure 14-14 below.

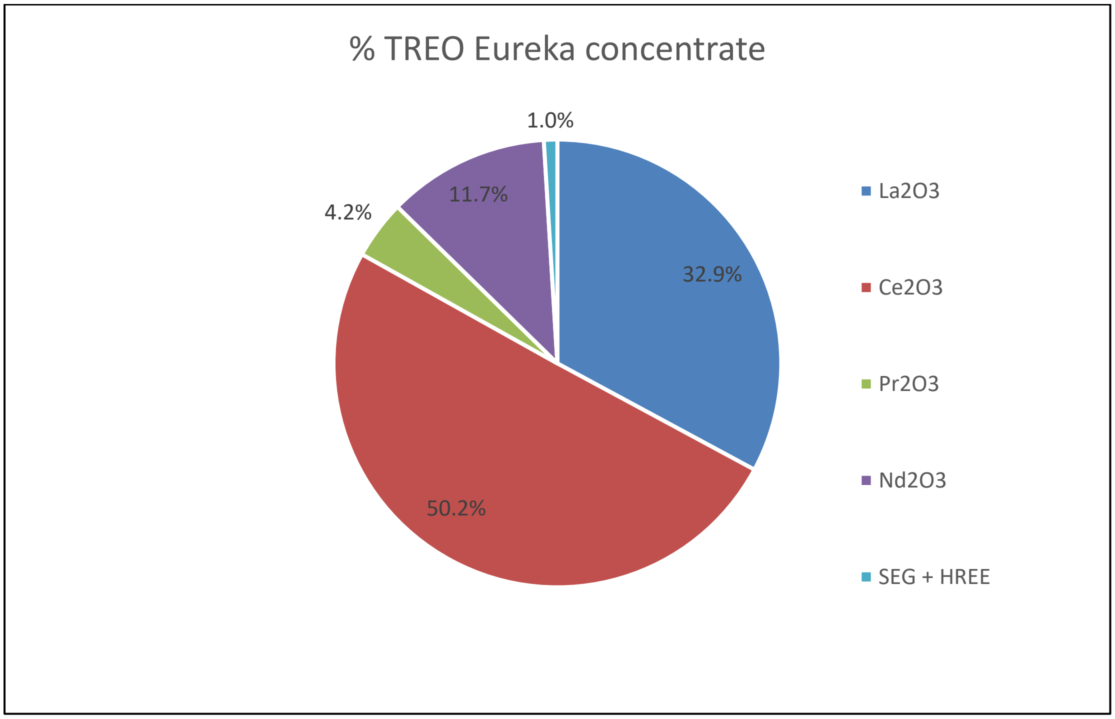

Figure 14-14: Proportion of REOs in Eureka concentrate.

The basket price for Eureka TREO used in this ITR is based on the average of prices between January 2018 and July 2019 based on records available from Argus Metals; the price being based on 99.5% – 99.9% pure separated REO products FOB China. Table 14-10 illustrates the main value drivers in the Eureka product and how revenue per tonne of concentrate would be derived based on the assumptions described in the text above. The revenue so calculated is exclusive of duties, taxes and royalties (the latter is likely to be 2 or 3%).

Table 14-10: Eureka Basket Price and Revenue Calculation

REO	Market price (USD/kg)	Proportion of Eureka TREO	Value Contribution to 1 kg Eureka TREO (USD)
Nd	46.0	11.7%	5.12
Pr	55.6	4.2%	2.34
Ce	2.0	50.2%	1.00
La	2.0	32.9%	0.65
M&HREO	-	1.0%	0.27

REO	Market price (USD/kg)	Proportion of Eureka TREO	Value Contribution to 1 kg Eureka TREO (USD)
Basket value 1kg TREO (USD)			9.39
			Concentrate Value Calculation
Basket value 1t TREO (USD)			9,390
Concentrate TREO grade			59%
Basket value 1t concentrate (USD)			6,100
Discount Factor Assumption			60%
Resultant Payable Value (USD / t concentrate)			2,440

The pit optimisation parameters used are summarised in Table 14-11 below.

Table 14-11: Pit optimisation parameters

Parameter	Units	Value
Geotechnical		
Overall Slope angle	Degrees	55
Mineral Recovery		
Mineral Recovery to 59% TREO concentrate	%	70
Mining Loss and Dilution		
Mining Loss	%	0
Mining Dilution	%	20
Operating Costs		
Mining	USD/t moved	5
Processing	USD/t milled	25
Transport and port handling	USD/t concentrate	7
General & Administration	USD/t milled	6
Basket Price		
TREO (9,390 plus 30% premium)	USD / t_{TREO}	12,207
Discount factor applied to contained TREO (assuming monomineralllic and 60% TREO grade)	%	60
Government Royalty	%	3

The optimised pit shell and the block model colour coded by classification status are shown in cross-section view in Figure 14-15 where green blocks that exceed cut-off grade are classified as Inferred Mineral Resources and grey blocks are excluded from Mineral Resource being below the pit or too far from sampling to be included in the Mineral Resource at present. Some 1% of blocks inside the pit are more than 50m away from sampled intervals.

The optimised pit is larger and deeper in Zone 1 due to there being multiple dykes with grades exceeding 4% TREO, the pit flows round to Zone 2 where the single dyke carries a similar grade at its eastern end.

In Zone 3 the pit is limited to a depth of some 5 m, due to the grade in the dyke being between 2% and 4% TREO. In other areas where dykes are lower grade, there is no pit shell developed.

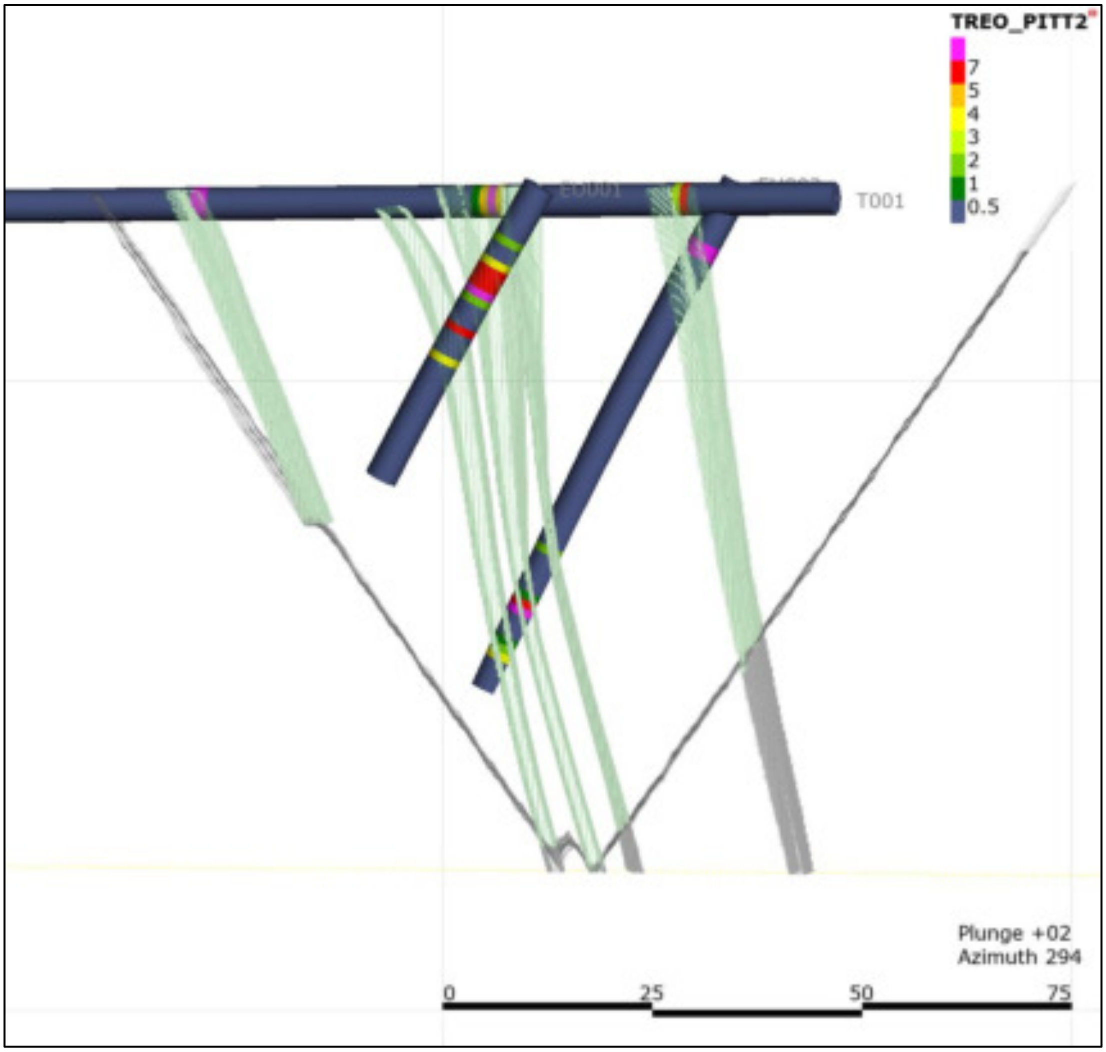

Figure 14-15: Cross Section of pit shell and resource classification in Zone 1

14.10.3 Reporting cut off grade

When assessing reasonable prospects for eventual economic extraction and determining a suitable reporting cut-off grade, it is normal practice to apply a premium to commodity price to ensure the Mineral Resource captures mineralisation that has potential to become economic rather than just that mineralisation already demonstrated to be economic. In this case therefore SRK has applied a 30% increase to the average REO prices over the period of January 2018 to July 2020.

SRK's reporting cut-off grade is the in-situ grade that generates sufficient revenue, based on the premium price, to cover the marginal operating costs which are those incurred after hauling ore to surface and getting product to point of sale. The cut-off grade for Mineral Resource reporting applied to the in-situ grades in the block model accounts for an estimated 20% grade dilution as a result of mining. On this basis SRK's reporting cut-off grade is 1.3% TREO.

14.11 Mineral Resource Statement

The maiden Mineral Resource statement in this ITR is dated 02 February 2021 and has been reported in accordance with guidelines and terminology given in the December 2012 Australian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves prepared by the Joint Ore Reserves Committee of the Australian Institute of Mining and Metallurgy, the Australian Institute of Geoscientists and the Minerals Council of Australia ("the JORC Code").

The JORC Code is recognized under NI 43-101 as an acceptable foreign code that governs the estimation and disclosure of mineral resources and mineral reserves. The JORC Code uses mineral resource and mineral reserve definitions and categories that are substantially the same as the CIM definitions mandated in NI 43-101, and also use mineral resource and mineral reserve categories that are consistent with the International Reporting Template, published by the Committee for Mineral Reserves International Reporting Standards ("the CRIRSCO Template").

The Mineral Resource statement has been prepared by Mr Martin Pittuck, CEng., MIMMM, FGS who is a Competent Person according to the definition given in the JORC Code and a Qualified Person as defined in NI 43-101. Mr Pittuck is a full-time employee of SRK and is independent of Battery Road, E-Tech Metals Ltd. and their subsidiaries.

SRK has reviewed the data collection, geological modelling and block modelling undertaken by E-Tech Namibia and their consultants and determined that there are reasonable prospects for eventual economical extraction based on

- benchmarked cost parameters;
- a review of prevailing metal prices;
- a review of E-Tech Namibia's expectations with respect to concentrate quality and pricing discounts;
- a preliminary pit optimisation based on the above; and
- the application of a 1.3% TREO cut off grade.

The Mineral Resource statement is given in Table 14-12 below.

Table 14-12: Eureka REE Project, Mineral Resource, February 2021

Category	**Tonnage (Kt)**	**Grade (%TREO)**	**of which NdPrO***
Measured	-	-	-
Indicated	-	-	-
Inferred	**310**	**4.8**	**0.7**

*the sum of the individual %Nd_2O_3 and %Pr_2O_3 grades

14.12 Grade-Tonnage Sensitivity

The sensitivity of the tonnage and grade above cut-off grade is illustrated below in Table 14-13 and Figure 14-16, this grade tonnage information is not a Mineral Resource statement.

Table 14-13: Tonnage and Grade Sensitivity

Cut off Grade (%TREO)	Tonnage above cut off grade (Kt)	Average Grade above cut off grade (%TREO)
0.0	325	4.6
1.0	315	4.8
2.0	275	5.2
3.0	235	5.7
4.0	210	6.0
5.0	155	6.5
6.0	85	7.3
7.0	65	8.4
8.0	40	9.1
9.0	10	10.0
10.0	5	10.6
11.0	0	11.4

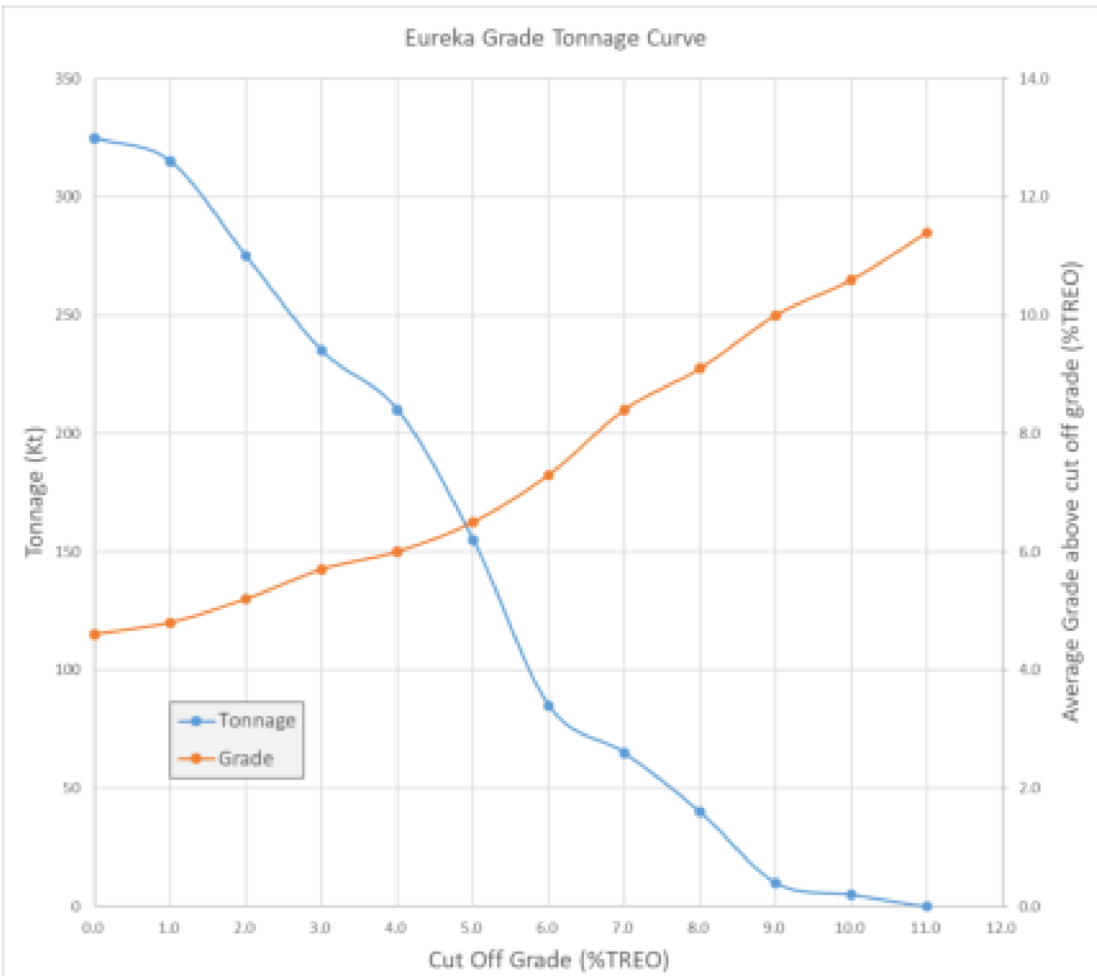

Figure 14-16: Grade-Tonnage Curve

14.13 Exploration Potential

SRK considers there to be good potential to increase the Mineral Resource. Notably:-

1. Despite some drilling and trenching 'misses' which may have been due to poor targeting / siting of trenches, there is some potential to extend the Zone 1 mineralisation westwards through the riverbed to join up with Zone 2.

2. There is potential to add a dyke to the model based on existing intersections in T028, EU007 and EU006.

3. Based on recent trenching, there is also potential to extend some of the dykes eastwards in Zones 1 and 3 and to find new dykes in the south part of Zone 1;

4. The carbonatite outcrops southwest of Zone 2 should be sampled.

5. Trenches 023 and 024 to the north of Zone1 and Zone 2 warrant some follow up trenching.

6. The area to the east of Zones 1 and 3 including Zone 4 should be comprehensively mapped with a view to identifying additional trenching targets.

7. The wider licence area should be covered initially with ground or airborne geophysics to build the geological picture and potentially identify other prospects.

Figure 14-17 below shows the wider exploration potential mentioned in points 8 and 9 above. The block model is shown in yellow and the parts of the model which provide the Mineral Resource are located in the pit rims shown as grey lines. The background is coloured based on the radiometric survey results showing total counts per second. The higher values (pink-red-orange-yellow) have the best potential to represent buried carbonatite dykes, although the large area of high values in the southern part of the image are understood to represent a large granite body. Thin red lines represent an interpretation of possible dykes based on the radiometric anomalies and the general trend of dykes delineated in the Mineral Resource. The low (blue) values may represent unmineralized host rocks or thick alluvial cover masking an underlying signal as is the case in the riverbed between Zones 1 and 2.

Existing trenches are shown as white lines and proposed trenches are shown as black lines. The thick brown line represents the area in which surface mapping has been concentrated to date, outside of this some reconnaissance work has been completed but comprehensive mapping has not yet been undertaken.

The inset image in the lower right corner represents the total licence area; this highlights the relatively small area on which work has been conducted to date.

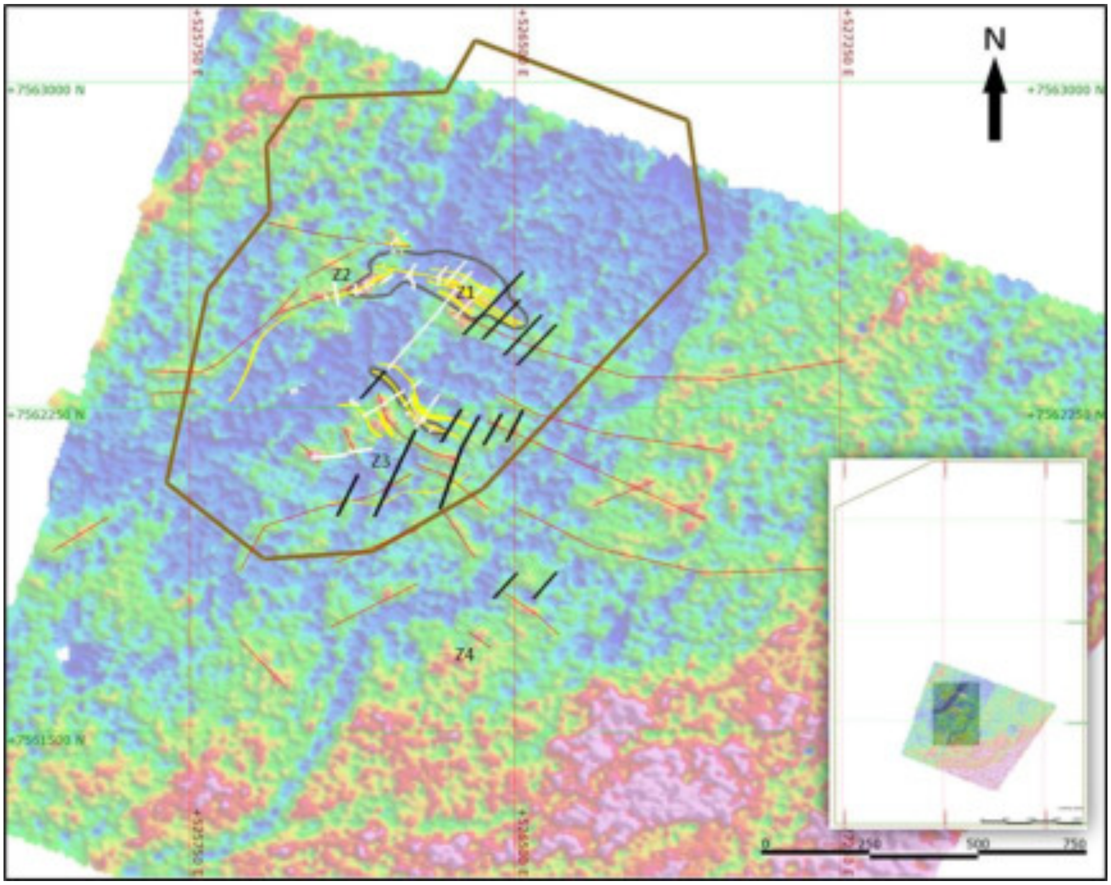

Figure 14-17: Plan view of wider exploration potential

By considering the Mineral Resource tonnage and its relationship to dyke outcrop metres, it is possible to start to quantify exploration potential associated with the length of radiometric anomalies. There are some 1,200 m of linear dyke outcrop within the pit rim used to constrain the Mineral Resource which equates to roughly 250 t of Mineral Resource per metre of dyke outcrop. This could be higher where there are multiple dykes such as found in Zone 1.

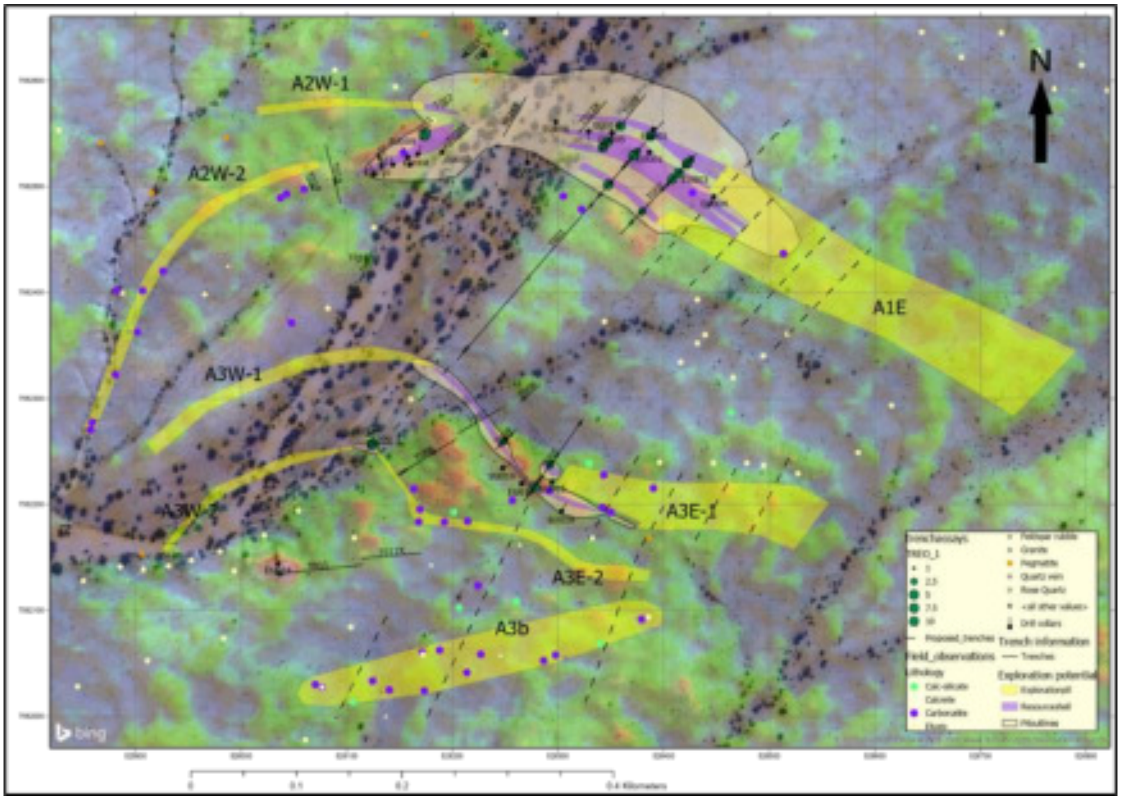

Figure 14-18: Near-resource exploration potential

There are some 2,400 strike metres of target anomalies identified in Figure 14-18. Additionally, in Figure 14-17, the linear anomalies to the east of the currently mapped area provide some 2,000 metres of exploration target.

By assuming that the trenching of these targets results in dyke intersections with the same frequency and with similar thickness and grade to those in the area hosting the Mineral Resource, SRK has derived an Exploration Target as defined by the JORC Code of between 500 Kt and 1,500 Kt at an average grade of between 2% and 5% TREO. This is based on the ratio of tonnage to surface length of dykes in the Mineral Resource area, applying this to the combined length of radiometric anomalies, and then creating a range based on 50% success rate and 150% success rate.

It should be noted that these estimates of potential tonnage and grade are conceptual in nature, that there has been insufficient exploration in any case to define a Mineral Resource and that it is uncertain if further exploration will result in the target being delineated as a Mineral Resource.

15 ITEMS 15 TO 22 OF FORM 43-101F1

The Project is not considered an Advanced Property at this stage in accordance with NI 43-101 and therefore items 15 to 22 of Form 43-101F1 are not applicable to this ITR. The items include:

- Item 15: Mineral Reserve Estimates
- Item 16: Mining Methods
- Item 17: Recovery Methods

- Item 18: Project Infrastructure
- Item 19: Market Studies and Contracts
- Item 20: Environmental Studies, Permitting and Social or Community Impact
- Item 21: Capital and Operating Costs
- Item 22: Economic Analysis
- Item 23 Adjacent Properties

No relevant information is available.

16 OTHER RELEVANT DATA AND INFORMATION

No other information is provided.

17 INTERPRETATION AND CONCLUSIONS

17.1 Current Status

E-Tech Namibia has previously completed cost effective exploration work on the Eureka Project resulting in a maiden Inferred Mineral Resource of 310 Kt at an average grade of 4.8% TREO which has reasonable potential to be economically exploited by open pit mining and small-scale mill and gravity circuits.

In terms of adding to the Mineral Resource, there are additional areas which warrant further mapping and trenching based on the area where geophysics has produced radiometric anomalies, and beyond this in the rest of the licence area. SRK has therefore also reported an Exploration Target of between 500 Kt and 1,500 Kt at a grade of between 2% and 5% TREO, as outlined further under Exploration Potential below.

It will be important for E-Tech Namibia to improve confidence in the technical-economic parameters influencing operating costs and revenue potential. It will also be important to develop capital cost estimates to which overall project economics will be quite sensitive given the small scale of operations suggested by results to date.

A number of technical-economic assumptions have been used to determine the Mineral Resource reporting criteria; these should be expected to change in future as dedicated studies, more detailed testwork and quoted estimates for certain costs are completed. The future trend of REE prices is not known and no attempt to predict this has been made, the Mineral Resource deliberately uses a premium on the average prices prevailing between January 2018 and June 2020; there is a risk that actual costs and revenues could be quite different from those presented in this ITR.

Overall SRK considers there is merit in undertaking the staged Phase 1 development programme outlined in Section 18.2 below.

17.2 Project Development

The Eureka deposit's combination of monomineralic REE-ore composition, potential for low-cost concentrate production through conventional gravity processing, and favourable deposit accessibility and jurisdiction, present an attractive REE sector investment opportunity.

While there remains considerable potential to increase the size of the deposit; it will be as important to de-risk the Project going forward by addressing the multidisciplinary aspects in a staged manner.

SRK believes there is good potential to increase the Mineral Resource on the Project through additional exploration and develop the many technical-economic aspects towards favourable outcomes. Inferred Mineral Resources have a low level of confidence by definition, and infill drilling with better quality sampling is required to increase the level of confidence and classify Indicated Mineral Resources in order to advance the Project to a Prefeasibility Study. Whilst SRK expects this to succeed, there is no guarantee that the Inferred Mineral Resources will be converted to Indicated Mineral Resources following infill drilling.

The technical-economic parameters presented in this report, in determination of the Mineral Resource estimate, are mostly conceptual and they may change significantly as the work progresses to improve confidence in them. The rare earth prices are based on a 2.5 year trailing average, these prices may increase or decrease in the future. The other assumptions around revenue, and price discounts in particular, are based on an understanding of what other producers in the industry are doing, E-Tech Namibia will need to develop its own arrangements in due course and these may be different for what is assumed in this ITR.

As a more detailed understanding is achieved and study milestones are reached, decisions to proceed to the next stage, or not, will be made. There is no guarantee that the Project will reach a successful outcome.

SRK is of the opinion that the E-Tech Namibia team has been prudent with plans and costs to date and has established relationships with employees and contractors which lend confidence to planning and budgeting at this stage.

18 RECOMMENDATIONS

18.1 Introduction

Following the milestone achievement of a maiden Mineral Resource estimate and the positive results from the initial metallurgical testing, it is recommended that the Project be advanced in a staged manner towards a Preliminary Feasibility Study ("PFS") contingent on results of each phase of work. This will involve further exploration, deposit delineation, metallurgical optimisation and further technical and economic studies.

It is recommended exploration be continued with the objective of infilling and expanding the sample coverage in and around the Mineral Resource model; some of this sampling has been completed with the 2020 and 2021 trenching and drilling; these samples now need to be assayed when new funds become available.

More widespread trenching and drilling should be conducted along resource model extension areas and in areas of untested radiometric anomalies and carbonatite outcrops. Diamond drilling has recently been introduced to provide core samples and better lithological and structural information from deeper intersections of the carbonatite and to provide geotechnical data and samples for comminution testwork. It is recommended diamond drilling be continued as infill to existing drilling which would allow for possible delineation of Indicated Mineral Resources.

18.2 Phase 1 Programme

Phase 1 of the development programme is sub-divided as follows to allow for periodic review in a reasonable timeframe:

18.2.1 Phase 1a: Continued Exploration and Mineral Resource Estimate Update

This phase includes:

- Maintaining environmental monitoring.
- Metallurgical test work on representative composite samples for continuing beneficiation optimisation work.
- Completion of core logging, core sampling and assaying of samples collected form initial diamond drilling completed for depth extent.
- Assaying of samples collected in the 2020-2021 trenching and drilling programmes.
- Updating of the Mineral Resource estimate and Technical Report.

18.2.2 Phase 1b: 12 month PEA programme, including:

- 2,500 m of trenching and mapping in the area to the east of Zones2, 3 & 4.
- Follow-up drilling and infill drilling: 4,000 m of diamond core drilling to test the depth extensions in Zone 1 and Zone 3, as well as selective infilling existing drilling whilst gathering structural and geotechnical data, based on results from Phase 1a.
- 3,500 m of RC Drilling to test the lateral and depth extent of newly identified targets, based on trenching results over Zones 2, 3 & 4.
- Regional early-stage exploration focused on identifying new areas of interest for possible further extension areas through field mapping, ground geophysics, ground truthing, trenching and initial RC drilling
- Metallurgical test work on material for continuing beneficiation optimisation work, based on results from Phase 1a.
- Marketing investigations to define the quality and specification of REE concentrate product and deliverable tonnages. Sending test material to interested offtake parties for independent assessment of price indicators. The potential of a value added intermediate “cracked” REE product to also be evaluated.
- Concurrent environmental monitoring and assessment, as well as stakeholder and community engagement.
- Updating of Mineral Resource Estimate targeting some Indicated Mineral Resources defined from the infill drilling, although there is no guarantee that this will be achieved.

- completion of a Preliminary Economic Assessment.
- Deploying remaining funds to progress PFS tasks, dependant on results.
  - conducting and confirming socio/environmental work
  - engineering studies for
    - surface infrastructure,
    - process plant and waste disposal designs.
  - If budget allows, further work could include concept/optmization studies for value adding mixed LREO production, or investment in other exploration targets in the wider property.

18.3 Phase 1 Project Development Budget

The proposed budget for Phase 1 is shown in Table 18-1.

Table 18-1: Phase 1 Development Budget

Phase	Timeframe	Description	Budget (CAD)
1a	Month 1 – 6	Completion of drilling programme, assaying of RC. Trenching and Diamond drilling samples	215,000
1a	Month 4-6	Updating of Inferred Mineral Resources and Technical Report.	85,000
1a-1b	Month 1-14	RC, Trenching and Core and sample storage	20,000
1a	Month 1-6	Assaying of samples collected in the 2020-2021 trenching, RC drilling and dd programmes.	352,000
1a-1b	Month 1-14	Wider early-stage exploration to identify new areas of interest for extension areas.	300,000
1-1b	Month 1-14	Follow up infill and extension drilling	150,000
1-1b	Month 1-14	Continued assaying and Metallurgical testing	185,000
1-1b	Month 1-14	Baseline Enviromental, ongoing monitoring and assessment	60,000
1-1b	Month 6-14	Compilation of updated resource	160,000
Sub-total			**1,527,000**
Corporate 1a-1c	Month 1-14	Working capital, administration, contingency	1,076,400
Total			**2,603,400**

Upon the successful completion of Phase 1, a follow up programme (“Phase 2”) will be required. Dependant on the results from phase 1, the Phase 2 program might include the completion of a PFS.

18.4 SRK Comments

The proposed Phase 1 programme will advance the geological understanding and test the additional geological potential considerably. Metallurgical testwork will also advance significantly, it will be important to not only develop the process methods and concentrate quality but also to test many samples representing different grades and rock types.

Overall, the staged programme represents a logical approach to fast tracking the Project development using an industry standard approach.

The proportion of budget for work done on the ground (as opposed to corporate overheads) will be approximately 60%.

signed

Keith Webb
Independent Consultant
(Exploration Geology)

For and on behalf of SRK Consulting (UK) Limited

signed

Martin Pittuck,
Corporate Consultant (Mining Geology),
Project Manager
SRK Consulting (UK) Limited

signed

Tim Lucks,
Principal Consultant (Geology),
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